

# EngrD 2190 – Lecture 6

Concept: Process Design Evolution by Incremental Improvement

Context: Example Exercises with Approximate Flow Rates  
(exercises 2.36 and 3.126 – solutions are posted)

Read Chapter 3 pp. 89-99 (mass balances)  
and Appendix C (significant figures).

Lecture 7 will follow the textbook. Bring pages 95-99  
to Lecture 7. Take notes by annotating **in color**.

# Active Learning Initiative Research Opportunity

- Cornell CBE is implementing active learning into the core ChemE curriculum.
- We seek your perspectives on learning, careers, and more! **We have sent a ~15-minute survey to your email** with the subject “Cornell CBE Active Learning Initiative Research Study Invitation”
- After you complete the survey, you will be contacted with the opportunity to participate in an interview at the end of this semester and receive a **\$25 gift card as compensation**. Please **complete the survey by 12/1/2025** to be eligible for this incentive.
- Please email Francis at [fl297@cornell.edu](mailto:fl297@cornell.edu) with any questions. Thank you for your support!



STRIDE

**CornellEngineering**

Smith School of Chemical and  
Biomolecular Engineering

# Writing Your Experience as Accomplishment Statements

- Your experience on a resume should not be a list of activities.
  - They should be **Deductive** statements.
- Experience written as accomplishment statements describe what impact your work had on the organization.
  - How were things improved through your work?
- Whenever possible, use metrics to describe your impact on the organization.

# Example

## Writing Accomplishment Statements

Average	Better!
Responsible for health promotion efforts.	Organized a company sponsored walk-a-thon which raised over \$8,000 for the American Heart Association and involved over 200 employees.
Handled bookkeeping for store.	Evaluated vendors and implemented an approval process for purchasing that reduced incidental expenses by 35%.
Performed filing and other clerical duties.	Re-organized and maintained over 350 technical files, thereby reducing the file search time by an average of three hours weekly.
Responded to customer inquiries and problems.	Earned the corporation's annual "Outstanding Service Provider" award based on feedback from both internal and external customers.

**Inductive**

**Quick gut check: At the end of each statement on a resume, ask 'so what?'**

# Examples in Process Design

Design Evolution  
by Incremental Improvements

*Solutions are posted*

## Exercise 2.36

**2.36** A good product  $G$  is produced by the following reaction:



Reactants available:    a liquid mixture of  $M$  (50 mol%) and  $X$  (50 mol%)  
                              a liquid mixture of  $E$  (50 mol%) and  $I$  (50 mol%)

Compound  $I$  is inert. In a mixture of  $M$ ,  $X$ ,  $E$ , and  $I$ , a side reaction produces by-product  $B$ :



Reactions 1 and 2 are highly exothermic. A mixture of 50 mol%  $M$  and 50 mol%  $E$  will explode. Likewise for  $X$  and  $E$ . To avoid explosion,  $E$  must not exceed 1 mol% if  $M$  and/or  $X$  are present.

All reactants and products are soluble in water. Water is inert to all reactants and products.

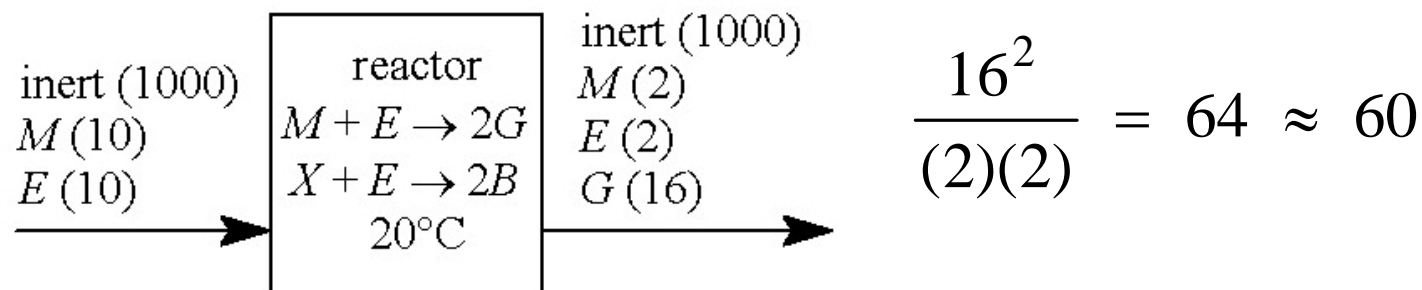
**Complication:** Cannot separate  $E$  and  $I$ .

## Exercise 2.36 – Reaction Details

Reactions 1 and 2 do not go to completion at the safe reaction temperature, 20°C. That is, if  $M$  and  $E$  enter a reactor, the amounts leaving the reactor will be such that

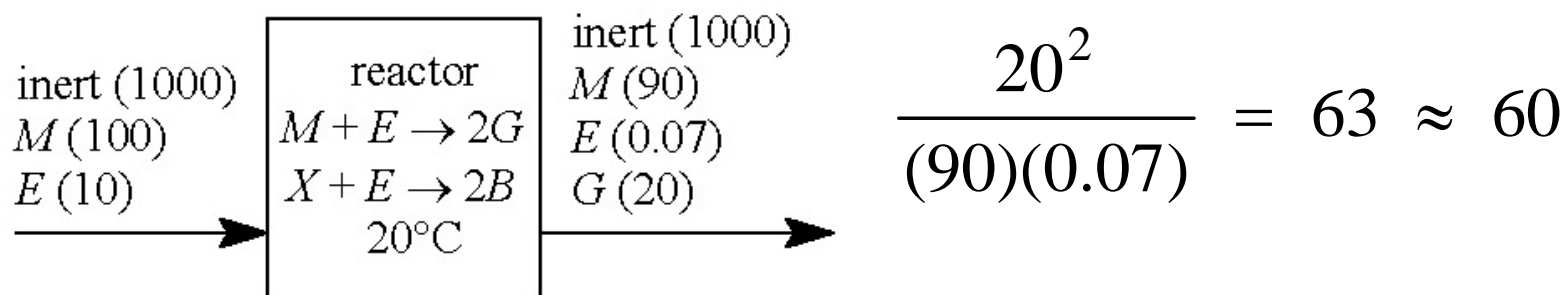
$$\frac{(\text{mol } G)^2}{(\text{mol } M)(\text{mol } E)} = 60 \quad \text{Deductive}$$

Two examples of reactor effluents are shown below. The first uses a stoichiometric mixture of  $M$  and  $E$ . The numbers in parentheses are flow rates, in mol/min.



Inductive

The second example shows a result when  $M$  is in excess.



Likewise if  $X$  and  $E$  enter a reactor, the concentrations leaving the reactor will be such that

$$\frac{(\text{mol } B)^2}{(\text{mol } X)(\text{mol } E)} = 60$$

## Exercise 2.36 – Goals and Rules

Design Goals (in decreasing importance):

- Maximize the yield of product  $G$  and any other marketable by-product(s).
- Minimize the yield of flow rate of the mixture of  $M$  and  $X$ .
- Minimize the number of units in your process.

Design Rules:

- Use 20 mol/min of the mixture of  $E$  (50 mol%) and  $I$  (50 mol%). You may use as much of the mixture of  $M$  (50 mol%) and  $X$  (50 mol%) as you wish.
- Indicate *approximate* flow rates of the substances in each stream. One significant figure is sufficient.

## Exercise 2.36 – Two Hints

Hint: In this exercise, the total number of mols is constant in both reactions. If a total of 20 mols of  $M$  and  $E$  enter a reactor, then a total of 20 mols of  $M$ ,  $E$  and  $G$  will leave the reactor. (Note - this is *not* a general principle.) Also, if a total of 100 mols of  $M$ ,  $E$ ,  $X$ , and  $I$  enter your process, then a total of 100 mols of  $M$ ,  $E$ ,  $X$ ,  $I$ ,  $B$ , and  $G$  must leave your process. Because  $I$  is inert, if 10 mol of  $I$  enter your process, then 10 mol of  $I$  must leave your process.

To calculate the flow rates of  $M$ ,  $E$ , and  $G$  in the reactor effluent, assume  $x$  mols of  $M$  and  $E$  react to form  $2x$  mols of  $G$ . For example, if 10 mol  $M$  and 10 mol  $E$  enter the reactor -

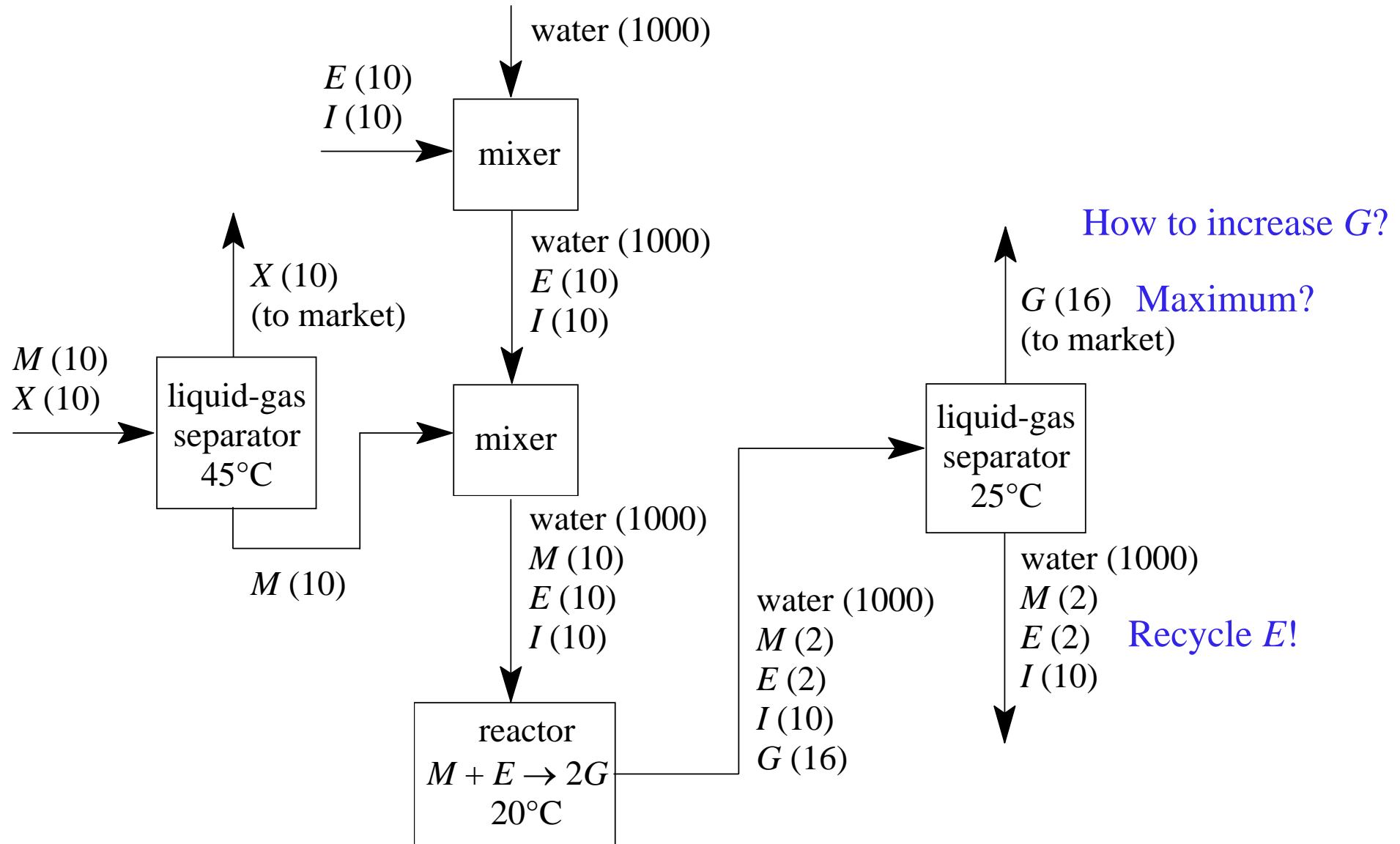
$$\frac{(\text{mol } G)^2}{(\text{mol } M)(\text{mol } E)} = 60$$

$$\frac{(2x)^2}{(10-x)(10-x)} = 60$$

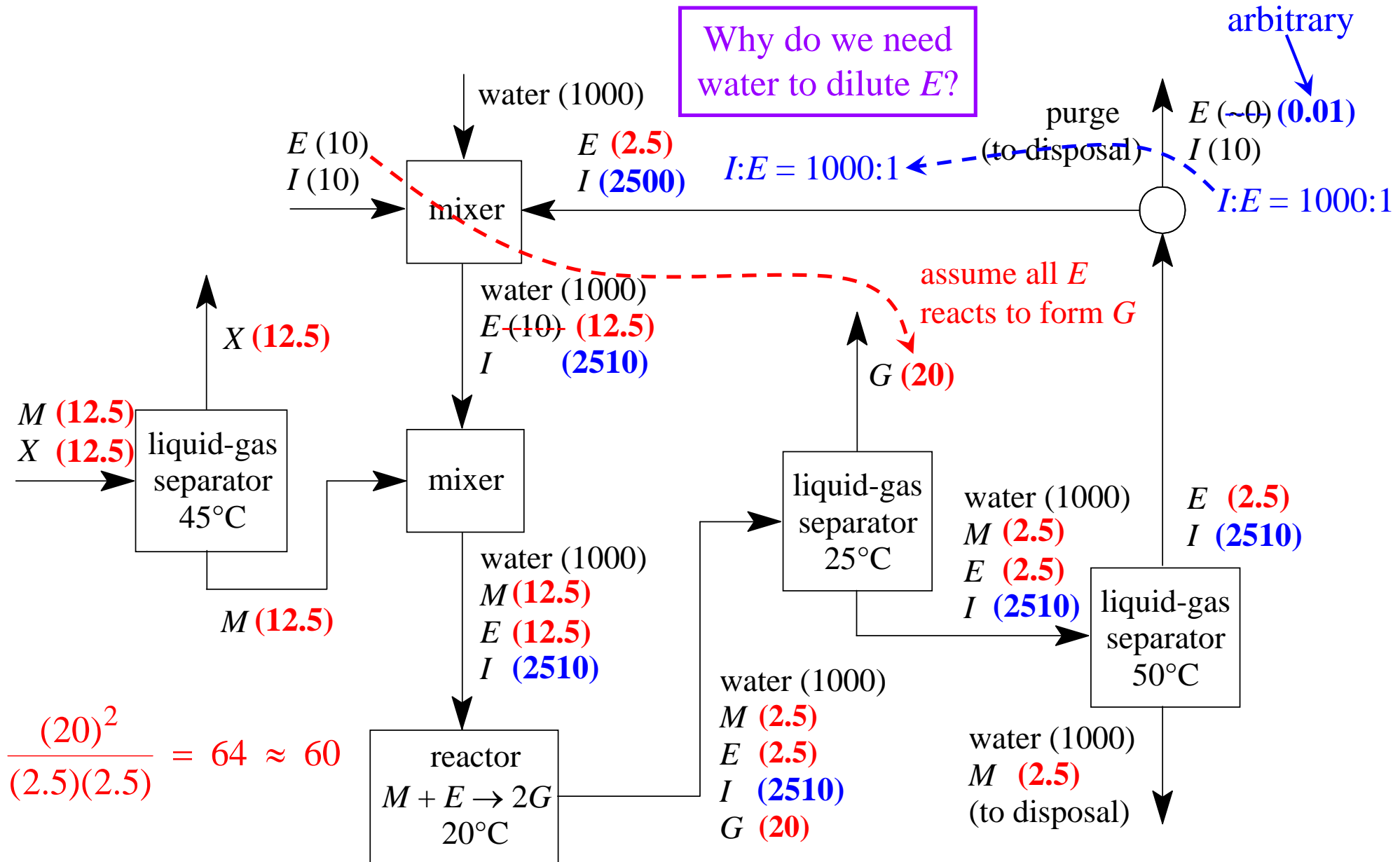
$$x \approx 8$$

Thus 2 ( $= 10 - x$ ) mol  $M$ , 2 ( $= 10 - x$ ) mol  $E$ , and 16 ( $= 2x$ ) mol  $G$  leave the reactor.

First attempt: Separate  $X$  from  $M$ , dilute  $E$  in water.

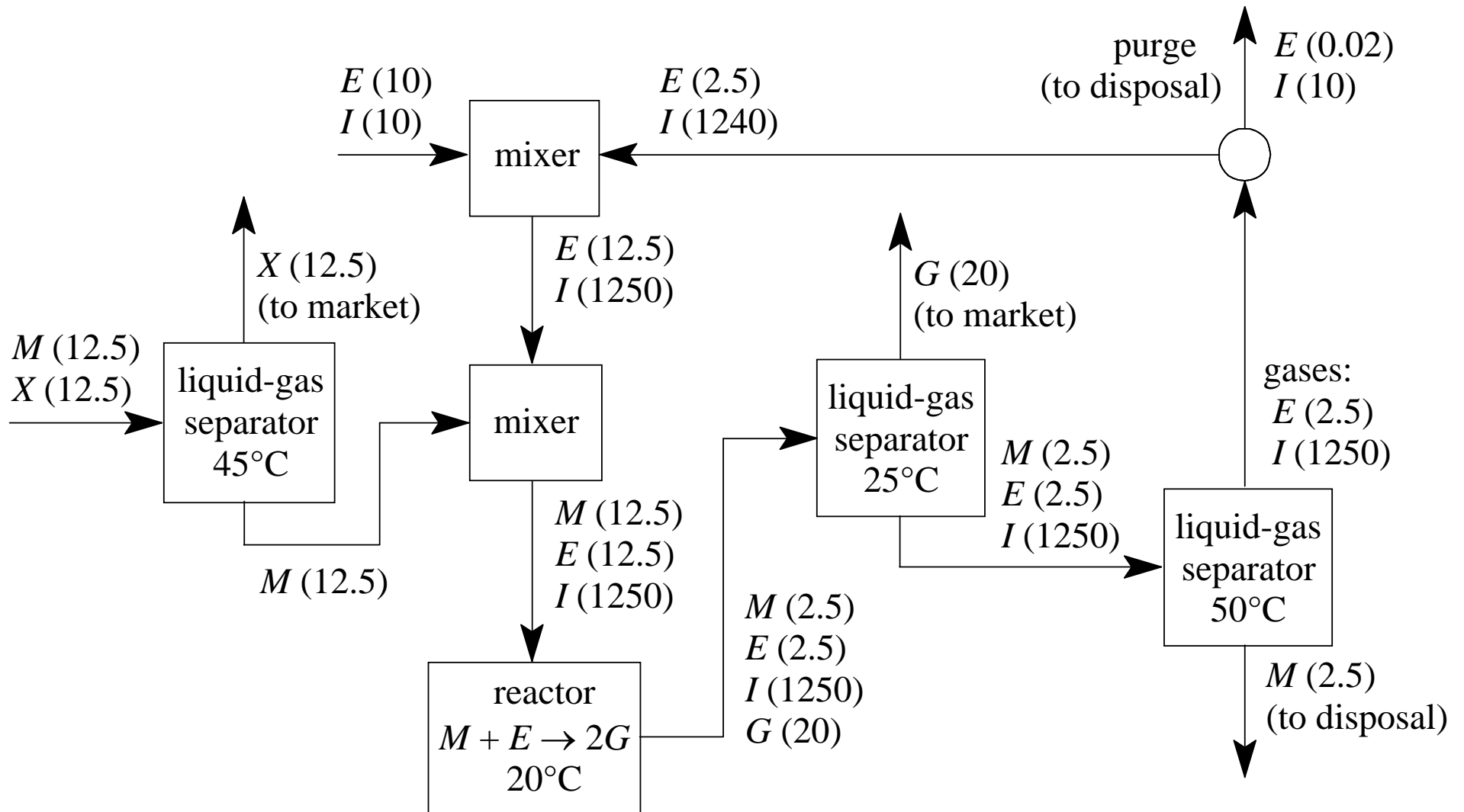


First attempt: Separate  $X$  from  $M$ , dilute  $E$  in water, recycle  $E$ .



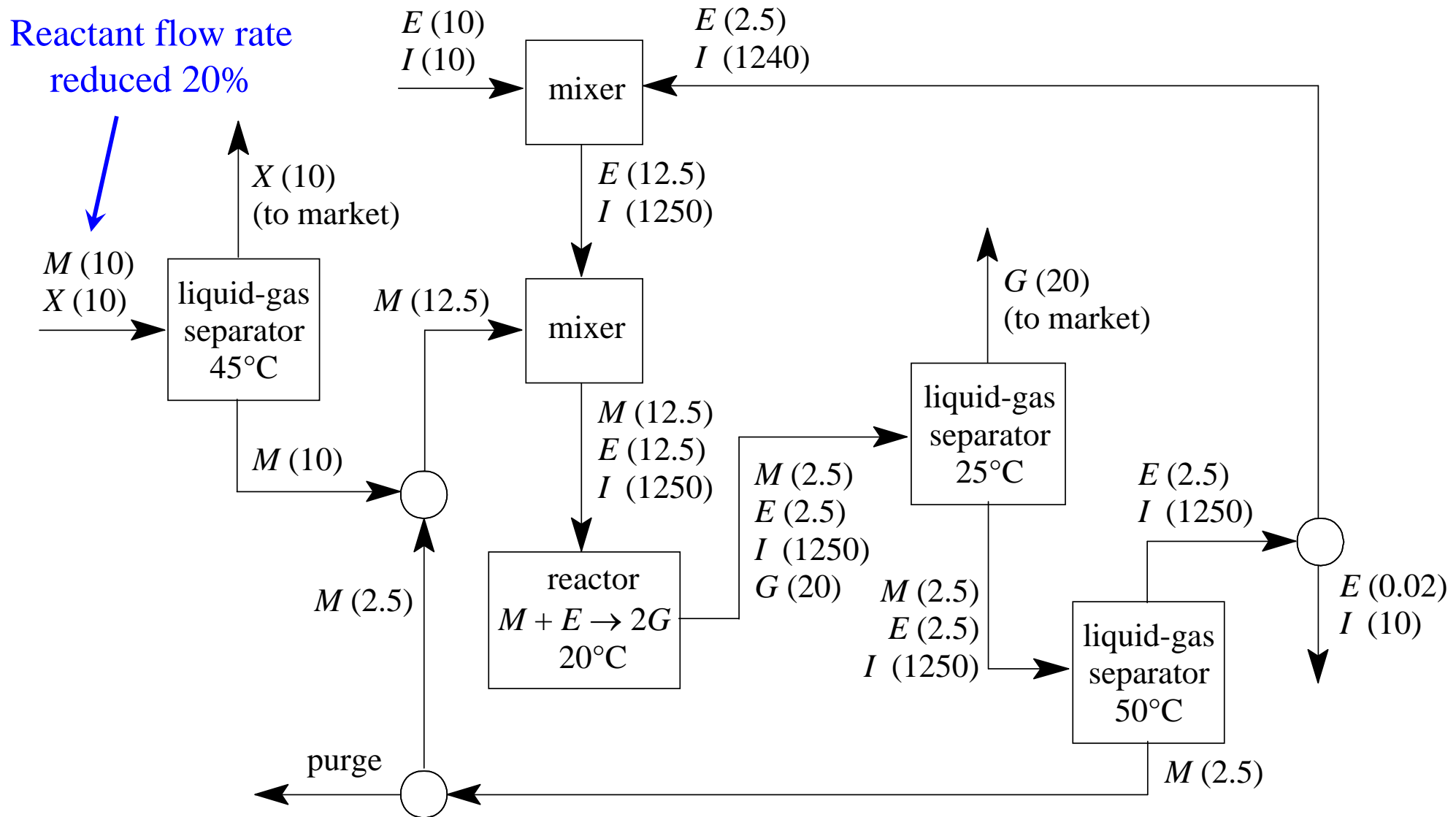
Purge a stream with a high concentration of impurity to minimize loss of desired substance(s).

2<sup>nd</sup> evolution: Use inert  $I$  to dilute  $E$ .

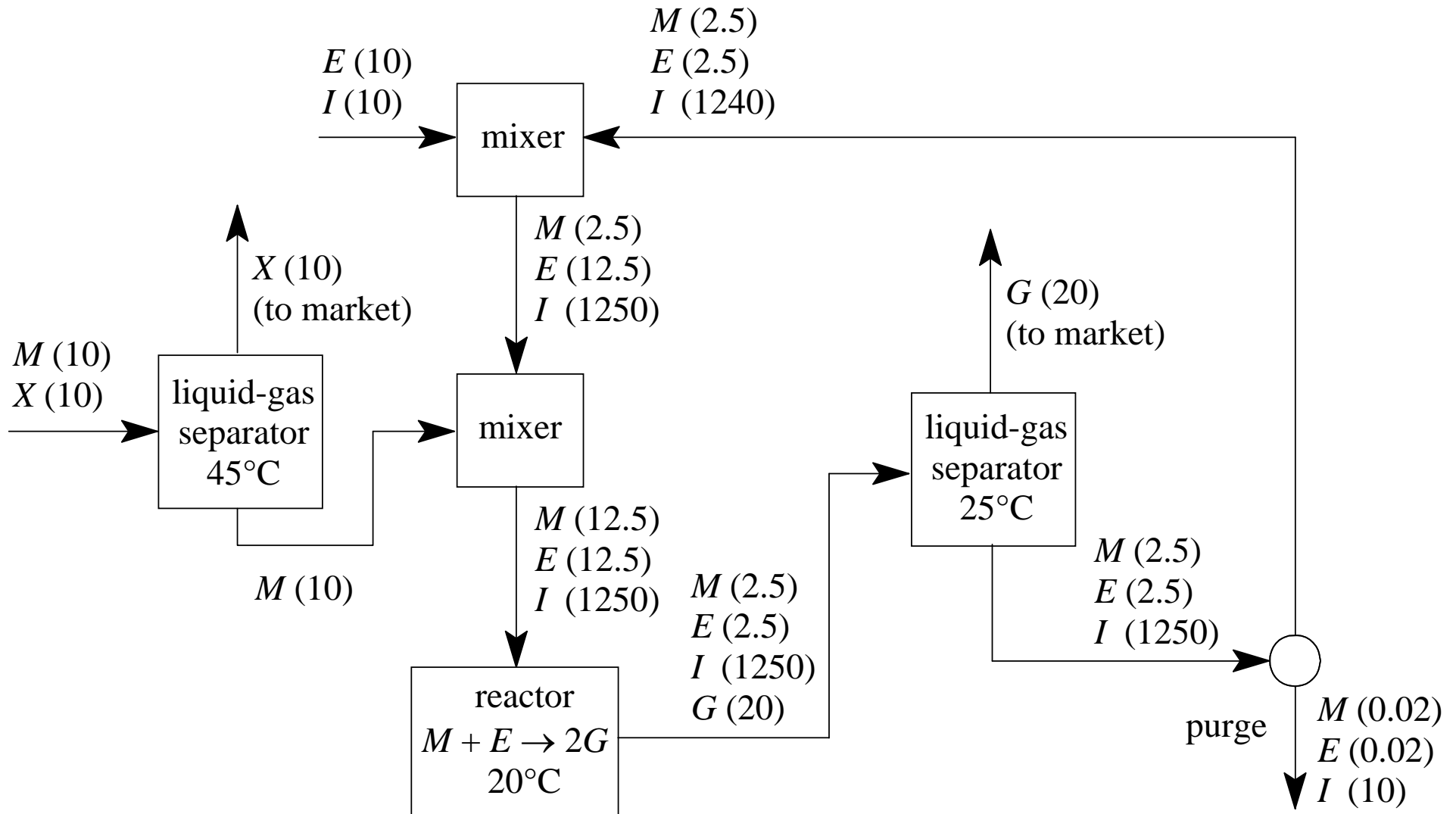


Waste treatment reduced  
to 2.5 mol/min  
from 1000 mol/min.

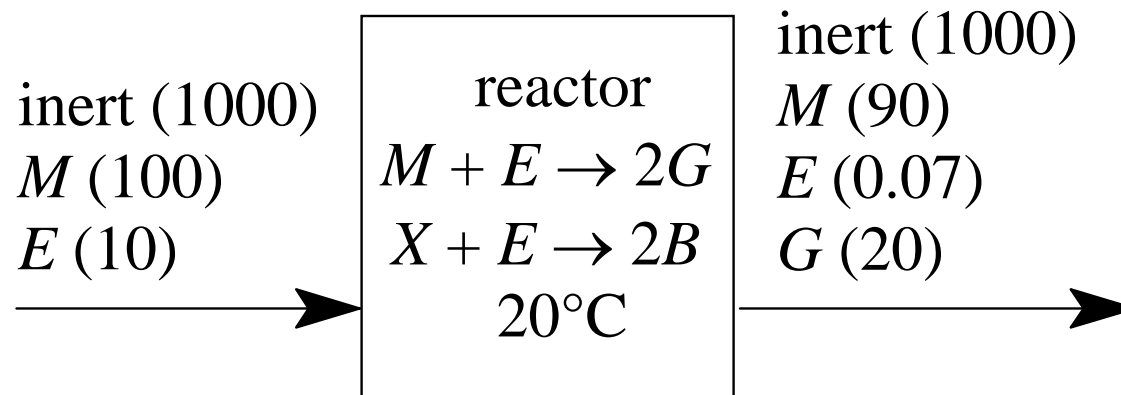
3<sup>rd</sup> evolution: Use inert  $I$  to dilute  $E$ , recycle  $M$ .



4<sup>th</sup> evolution: Recycle  $E$  and  $M$  without distillation.



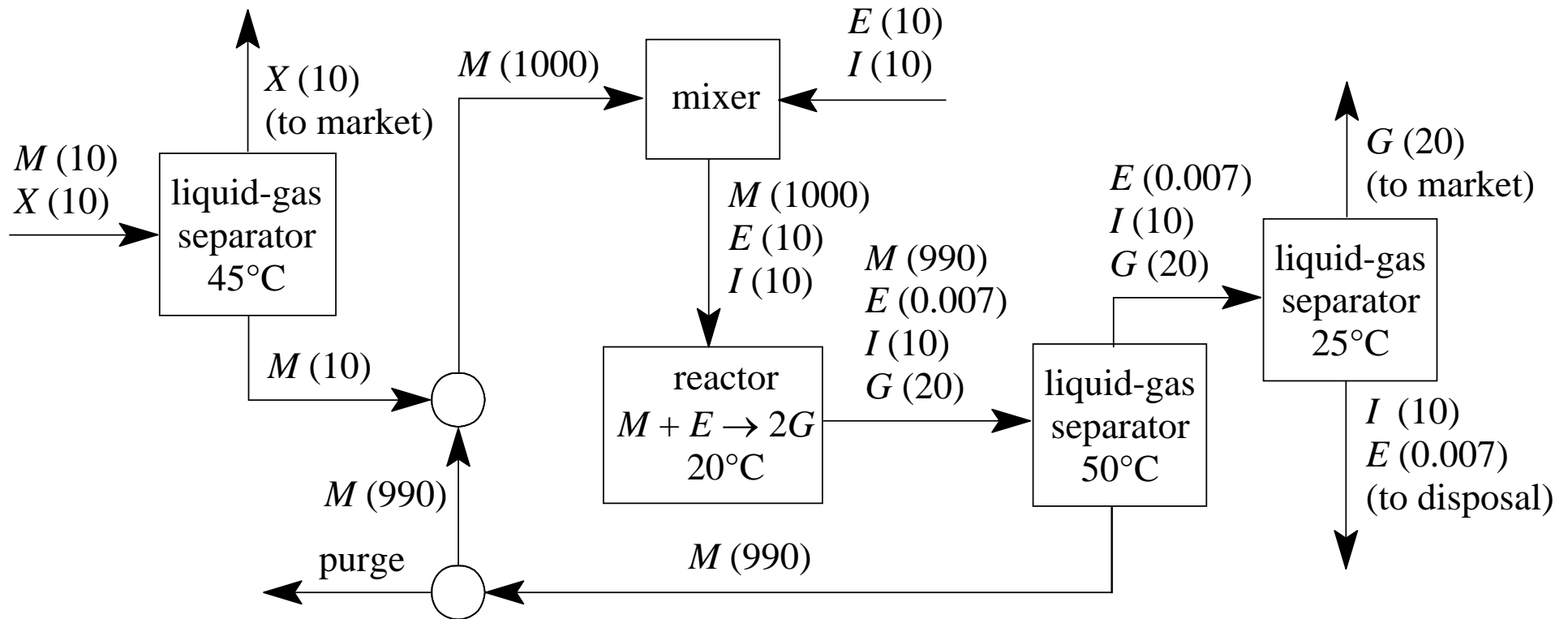
Next evolution hinted by the second example of reactor flow rates.



Excess reactant  $M$  can serve as the ‘inert’ solvent!

The amount of  $E$  in the reactor effluent  
(and thus the amount of  $E$  purged)  
can be decreased by excess  $M$  in the reactor!

5<sup>th</sup> evolution: Use  $M$  to dilute  $E$ .



Elegant!

## Exercise 2.36: Lessons Learned

Accumulate inert substances in a recycle loop to decrease ancillary losses in a purge stream.

When choosing a solvent, consider the requirements for the solvent. In this example, water is viable, but inert  $I$  is better, and reactant  $M$  is better yet.

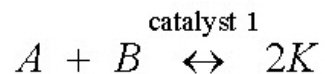
Start with a simple design and evolve by identifying the *real* problem.

## Example Exercise from Prelim 1, 2014.

**3.126** Design a process to obtain pure  $A$  from a mixture of  $A$ ,  $B$ , and  $I$ ;  $A:B:I = 11 \text{ mols}:2 \text{ mols}:1 \text{ mol}$ . Because  $A$ ,  $B$ , and  $I$  have the same melting point and the same boiling point, the mixture cannot be separated by physical means.

But  $A$ ,  $B$ , and  $I$  have different chemical reactivities.  $I$  is inert;  $I$  reacts with nothing.

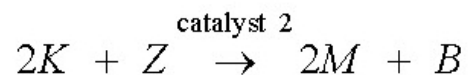
$A$  and  $B$  react to form  $K$ .



Reaction is at  $200^\circ\text{C}$  and requires the presence of catalyst 1.

Reaction is reversible and  $\frac{(\text{mol } K)^2}{(\text{mol } A)(\text{mol } B)} \approx 1$  in the reactor effluent.

$K$  reacts *irreversibly* with  $Z$  to produce  $M$  and release  $B$ .

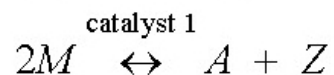


Reaction is at  $100^\circ\text{C}$  and requires the presence of catalyst 2.

For  $\frac{\text{mol } Z}{\text{mol } K} > 10$  in the reactor input, all  $K$  is consumed.

For  $\frac{\text{mol } K}{\text{mol } Z} > 10$  in the reactor input, all  $Z$  is consumed.

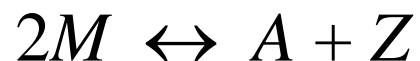
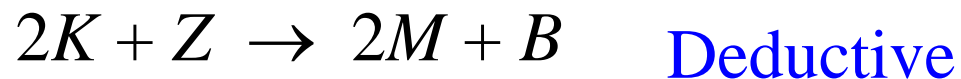
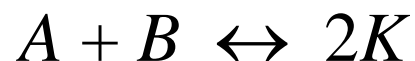
Finally,  $M$  decomposes reversibly to  $A$  and  $Z$ .



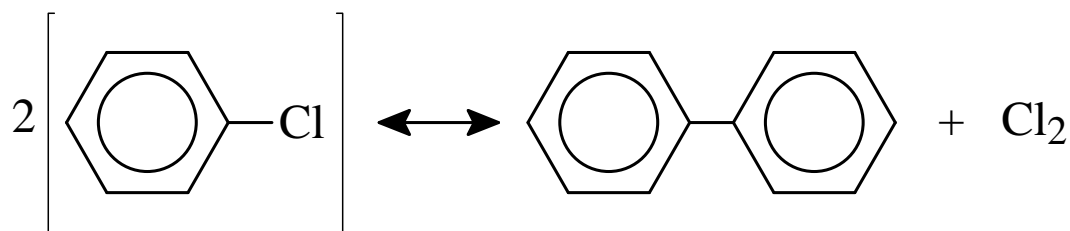
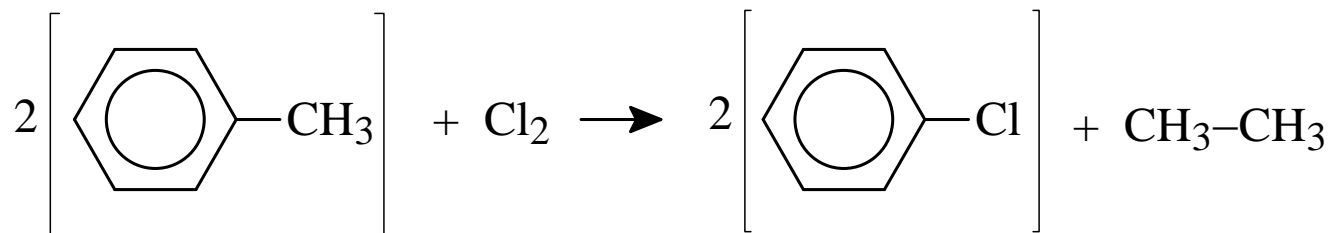
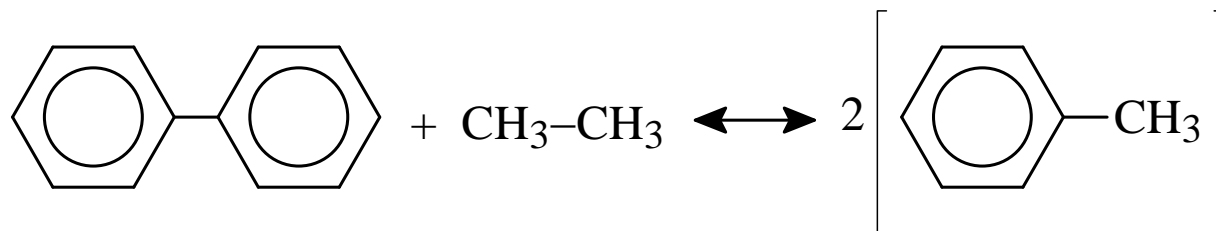
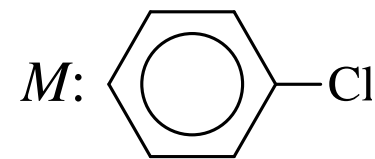
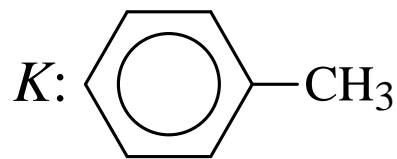
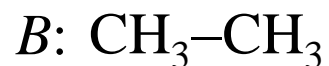
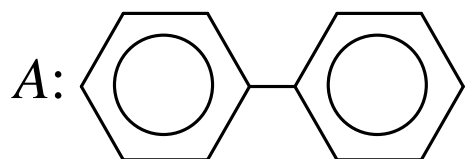
Reaction is at  $200^\circ\text{C}$  and requires the presence of catalyst 1.

Reaction is reversible and  $\frac{(\text{mol } M)^2}{(\text{mol } A)(\text{mol } Z)} \approx 1$  in the reactor effluent.

# Exercise 3.126 reactions



Here are some possible chemical components represented by *A*, *B*, *K*, *M* and *Z*, but wrong melting points, boiling points, and chemical reactions:



# Exercise 3.126 – Goals and Rules

## Design Goals (in decreasing importance)

Maximize the output of pure  $A$ . You must produce at least 10 mol/min of pure  $A$  for full credit.

Minimize the input of  $Z$ .

Minimize the *number* of units.

## Design Rules

Use 14 mol/min of the  $A+B+I$  mixture: 11 mol  $A$  + 2 mol  $B$  + 1 mol  $I$ .

You may use as much  $Z$  as you wish.

Use only one catalyst per reactor. The catalyst is a permanent part of a reactor. You need not add catalyst and there is no catalyst in the reactor output.

Liquid-solid separators produce wet solids.

## Exercise 3.126: Strategy to Maximize A

Convert  $A + B$  to  $K$ :  $A + B \leftrightarrow 2K$

Separate  $K$  from  $A$ ,  $B$ , and  $I$ .

React  $K$  with  $Z$ :  $2K + Z \rightarrow 2M + B$

Separate  $M$  from  $B$  and excess  $Z$ .

Recycle  $B$  to first reactor.

Convert  $M$  to  $A + Z$ :  $2M \leftrightarrow A + Z$

Separate pure  $A$  from  $M$  and  $Z$ . **Product!**

Recycle  $M$  and  $Z$  to separator in 2<sup>nd</sup> step.

## Exercise 3.126: Alternate Strategy

*Work backwards from the product.*

If we had pure  $M$ , we could convert  $M$  to  $A + Z$ .

Separate pure  $A$  from  $M$  and  $Z$ . **Product!**

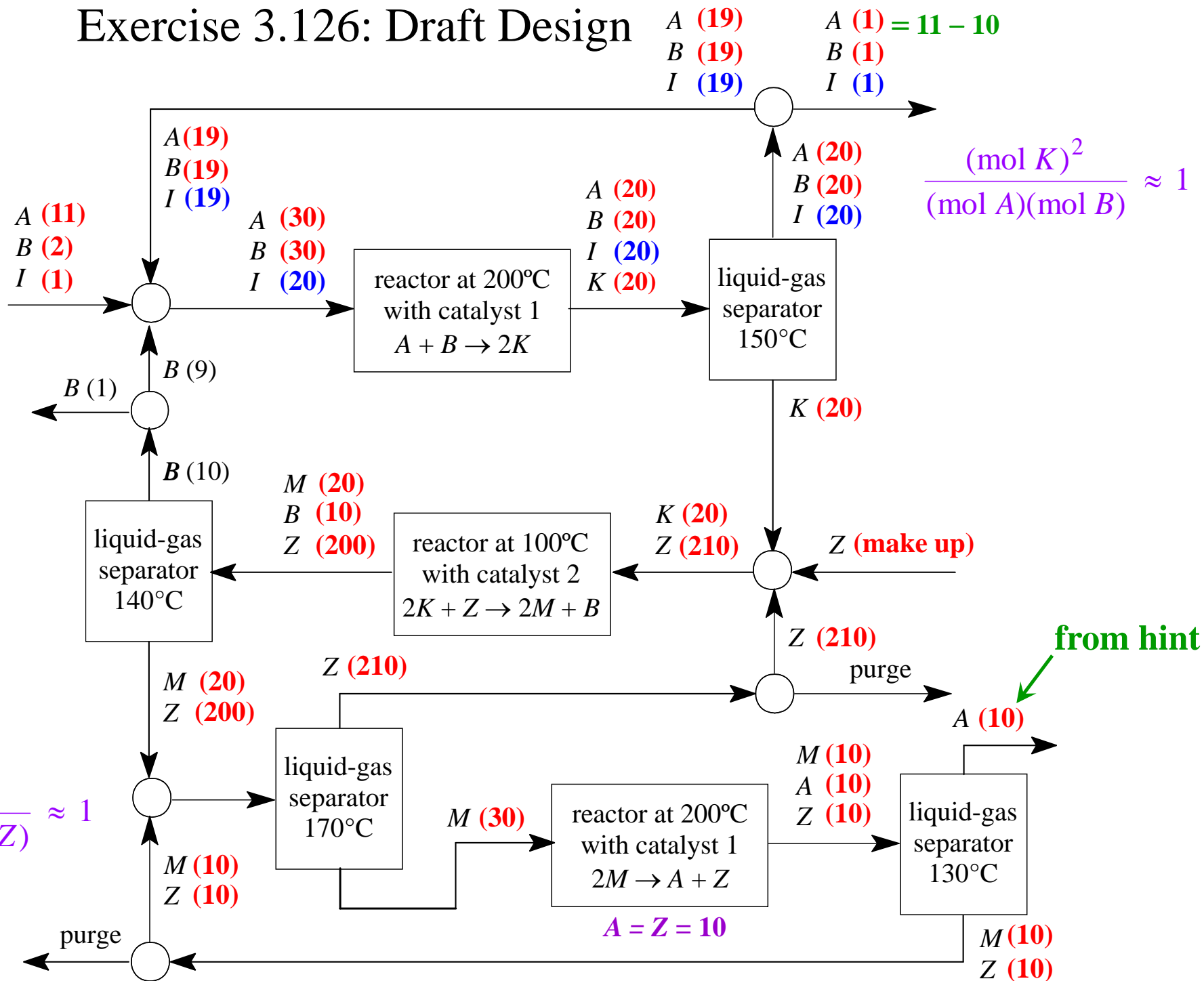
React  $K$  with  $Z$  to form  $M$  (and  $B$ ):  $2K + Z \rightarrow 2M + B$

Separate  $M$  from  $B$  and excess  $Z$ .

React  $A + B$  to form  $K$ :  $A + B \leftrightarrow K$

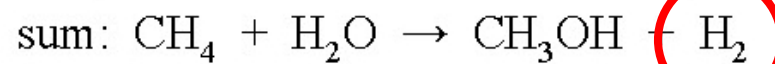
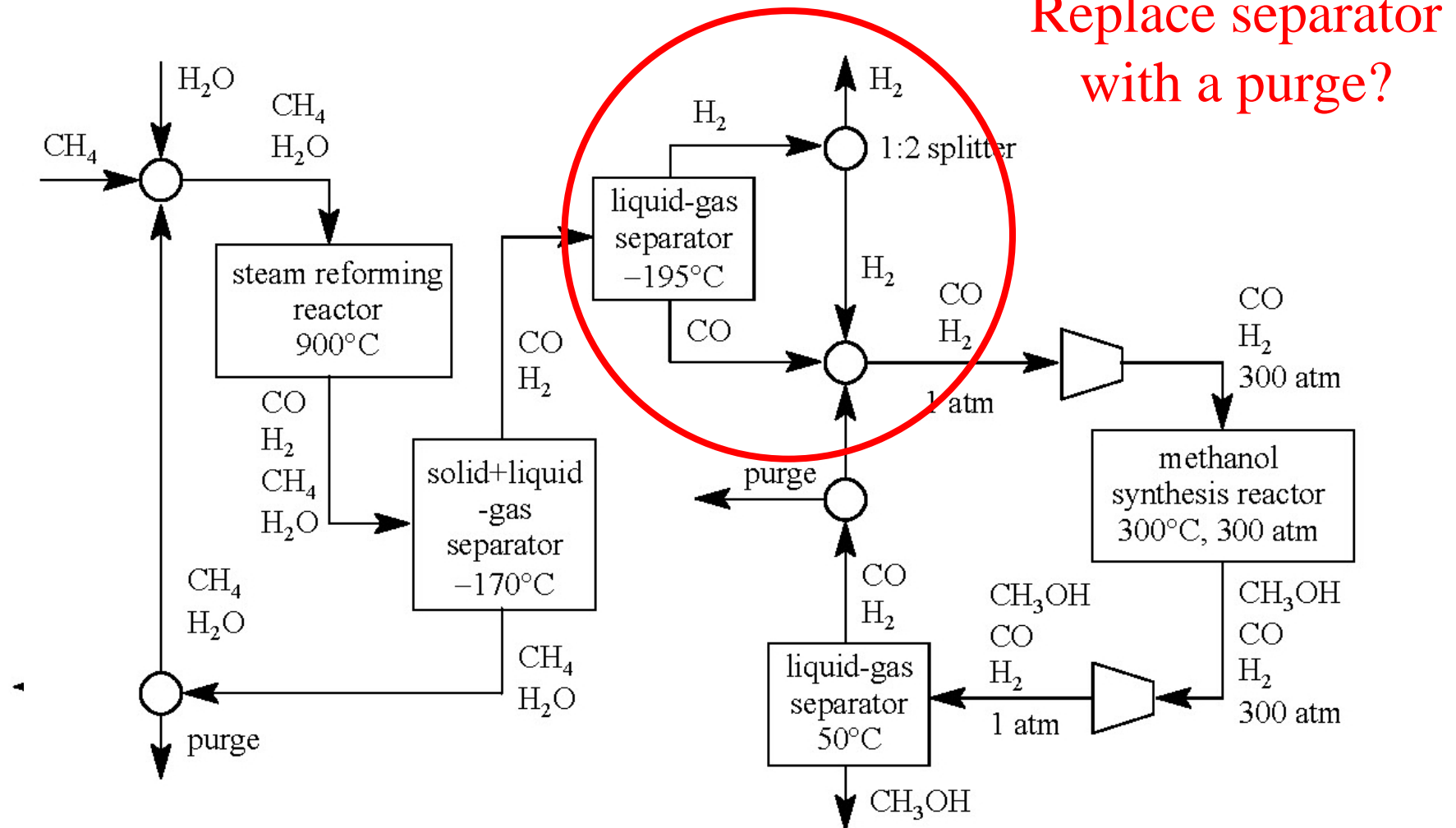
Separate  $K$  from  $A$ ,  $B$ , and  $I$ .

# Exercise 3.126: Draft Design



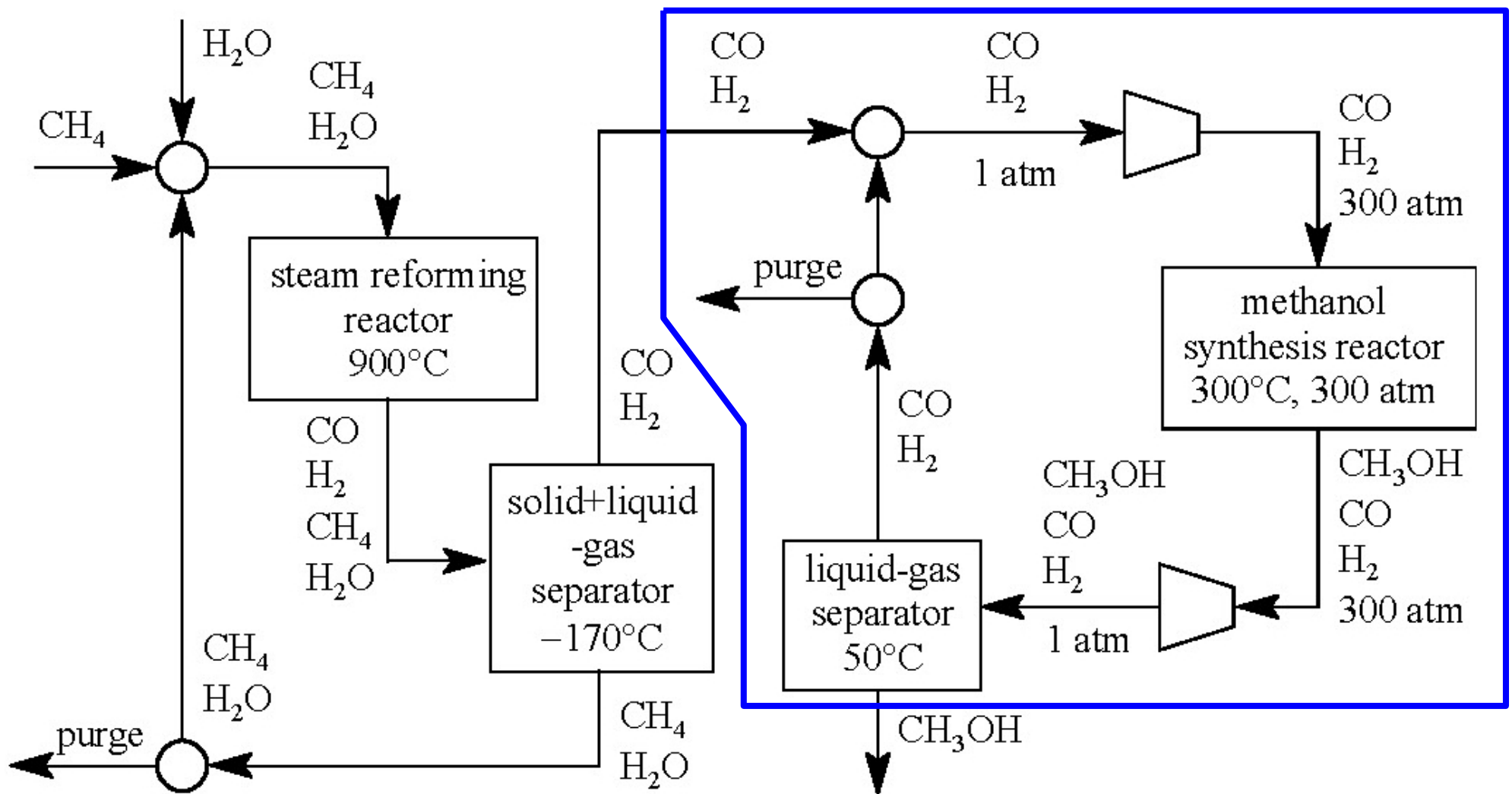
# Calculation Session 1 – Design Exercise 2.22(A)

## Convert CH<sub>4</sub> to CH<sub>3</sub>OH

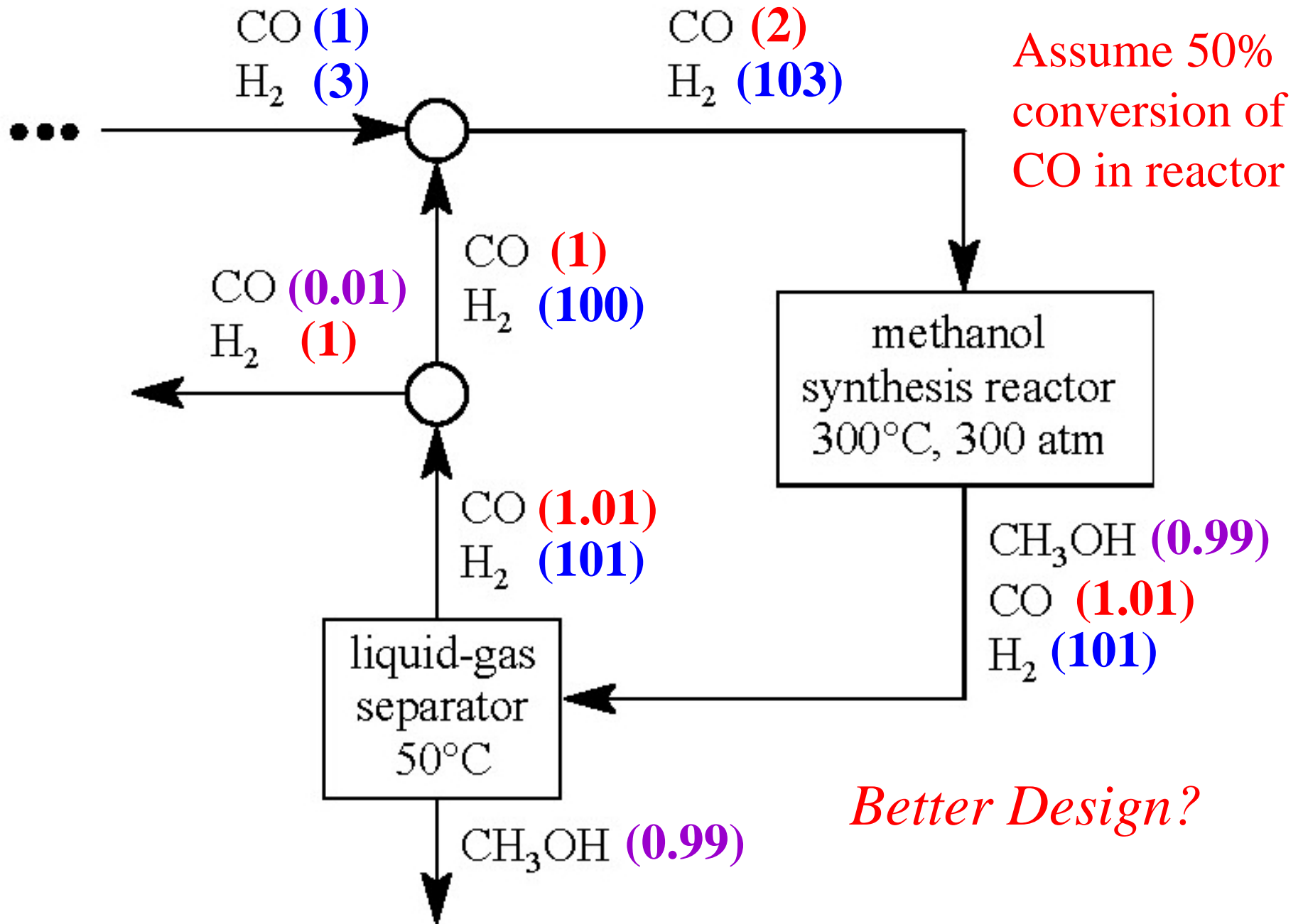


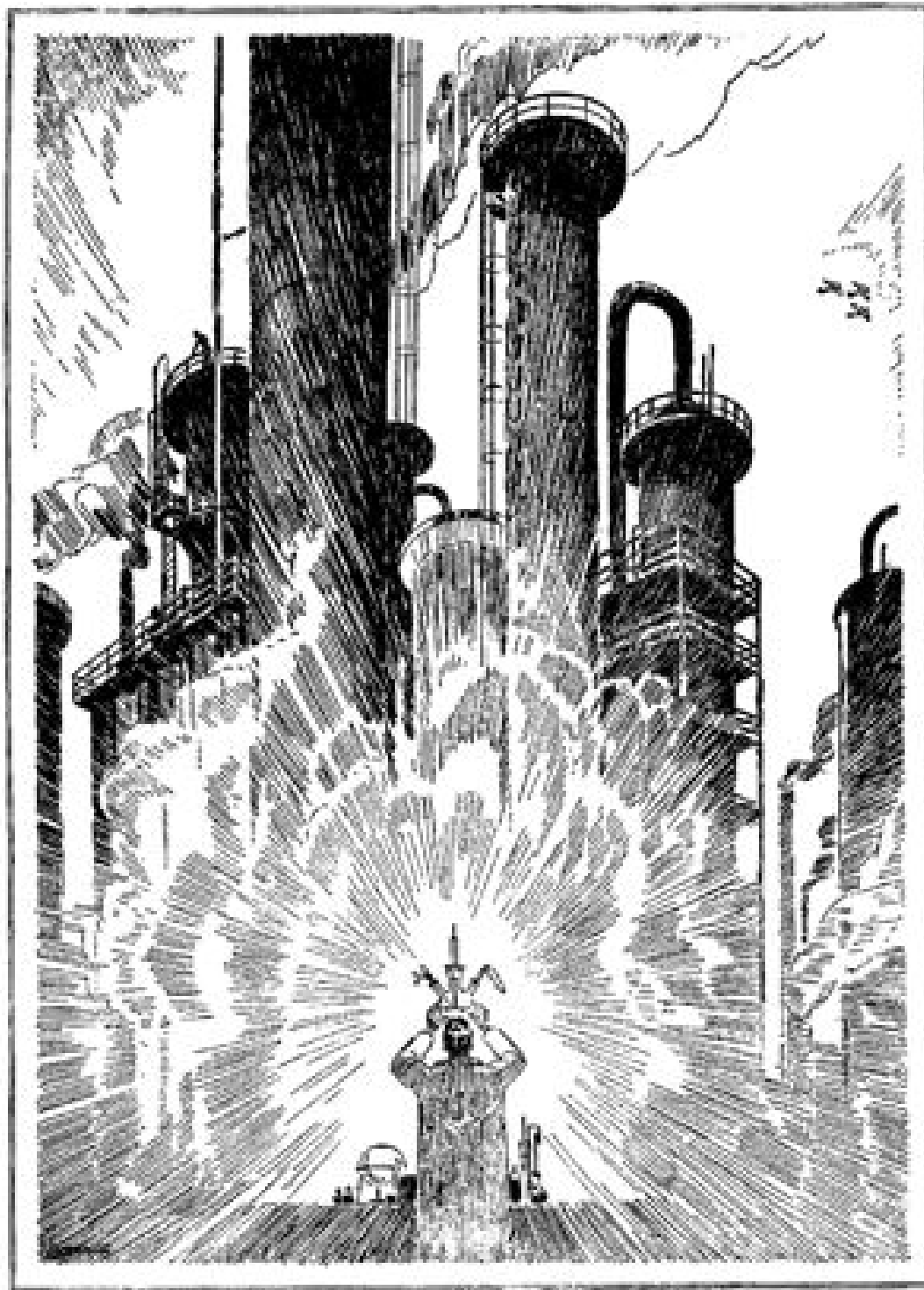
Must remove  
some H<sub>2</sub>.

## Exercise 2.22: How to remove $H_2$ via the purge?



## Exercise 2.22: How to remove H<sub>2</sub> via the purge?





Man in a Chemical  
World: The Service of  
Chemical Industry,  
A. Cressy Morrison (1937).  
Illustrator [Leon Soderston](#).



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