

EngrD 2190 – Lecture 8

Concept: Process Analysis – Mass Balances with Chemical Reactions

Context: Options for Unreacted Reactants:

Discard?

Separate & Recycle?

Recycle with Purge?

Defining Question: What are the two options for writing a mass balance on a system with chemical reactions?

Read Chapter 3 pp. 106-110 (mass balances with chemical reactions)

EngrD 2190 – Lecture 8

- Homework 2 due today at noon.

Write team code and names of all *contributing* team members on all solutions. Indicate this week's Team Coordinator.

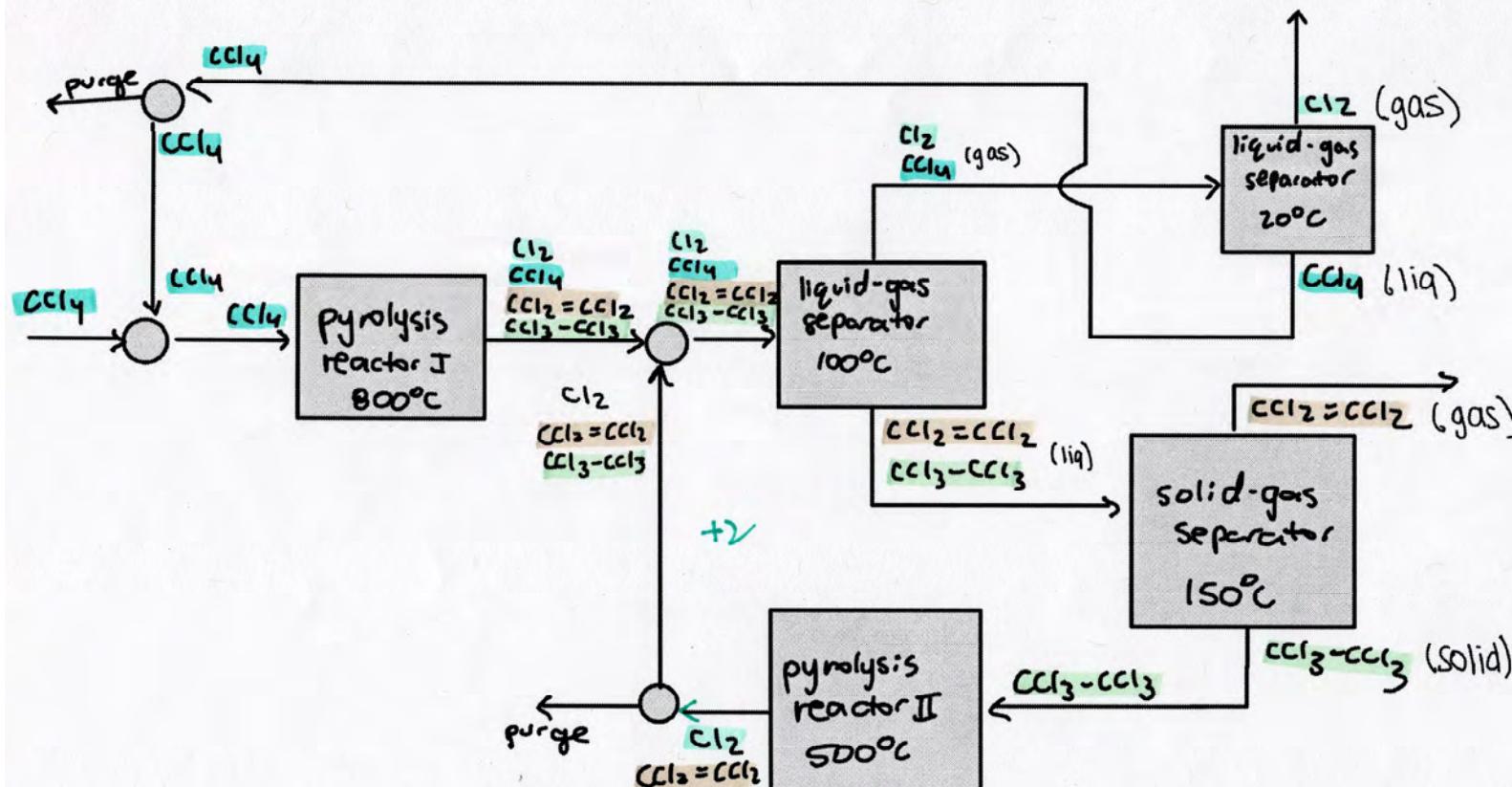
Submit *after* lecture or deliver to the EngrD 2190 mailbox in a cabinet in the hallway outside 116 Olin Hall (ChemE Business Office). **Not to my mailbox.**

Homework 1 Excellence – exercise 2.7 – Team 11

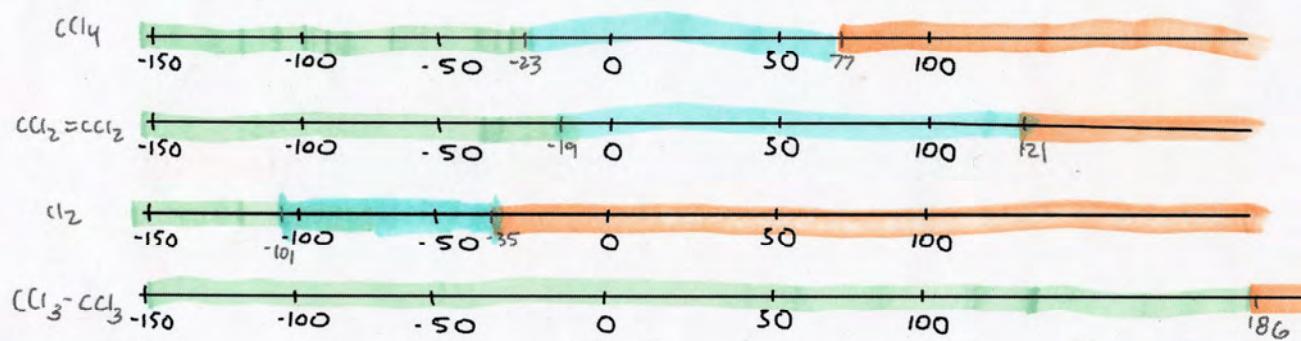
PROBLEM 2.7

Improvement #2:

TEAM 11
Week coordinator: Isabelle Bennie
Stefanie Jones
Anna Voronova



Style +2.



reactor out
e products
refine
+ 100 °C

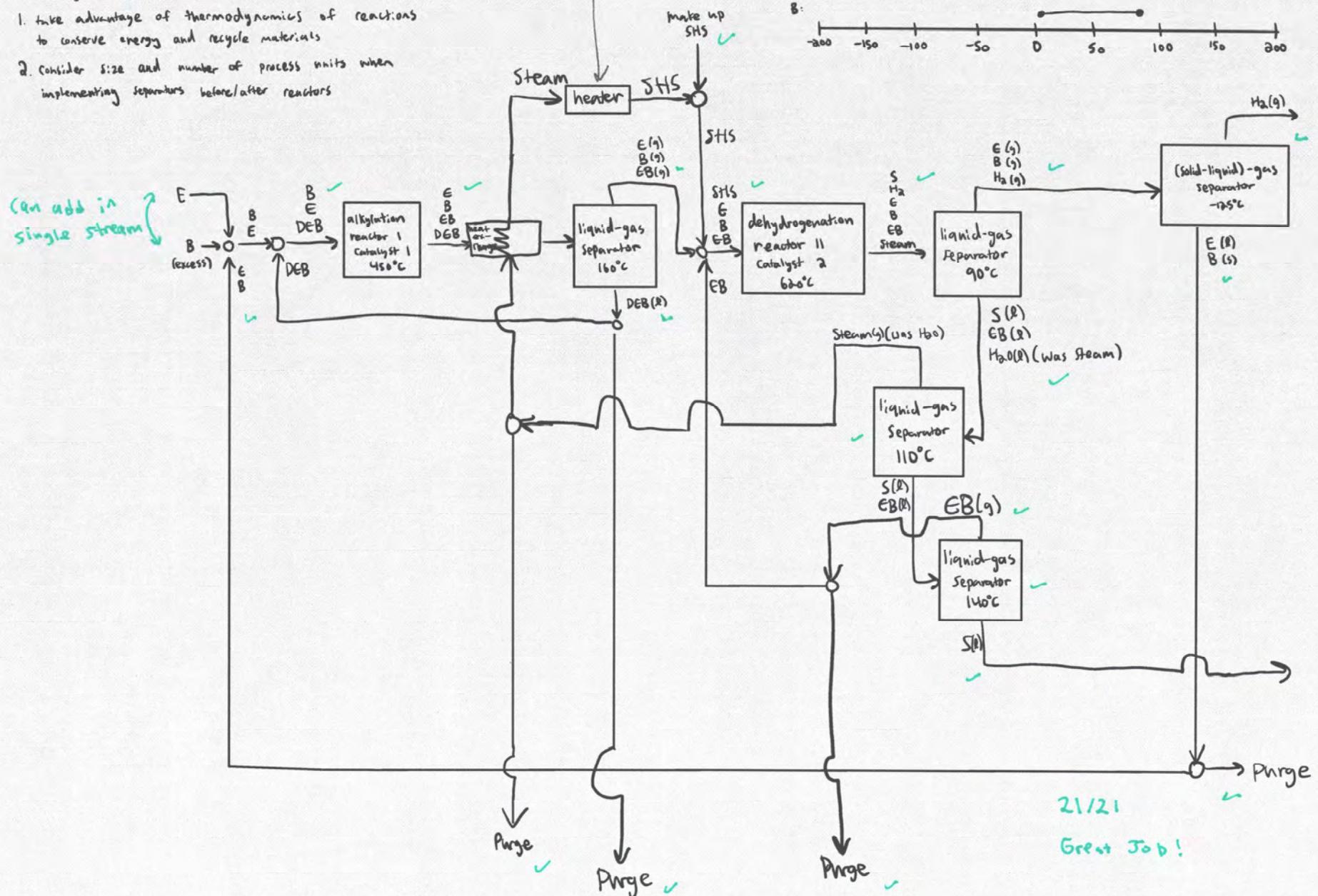
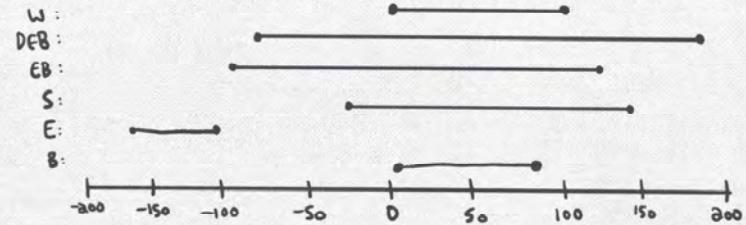
Homework 1 Excellence – exercise 2.24 – Team 6

2.24
Minwoo Chung
Bill Nguyen
Wilson Zhang

takeaways: ✓

1. take advantage of thermodynamics of reactions to conserve energy and recycle materials
2. consider S:2E and number of process units when implementing separators before/after reactors

✓
heater heats remaining
steam to S:2E that
was not by heat
exchanger

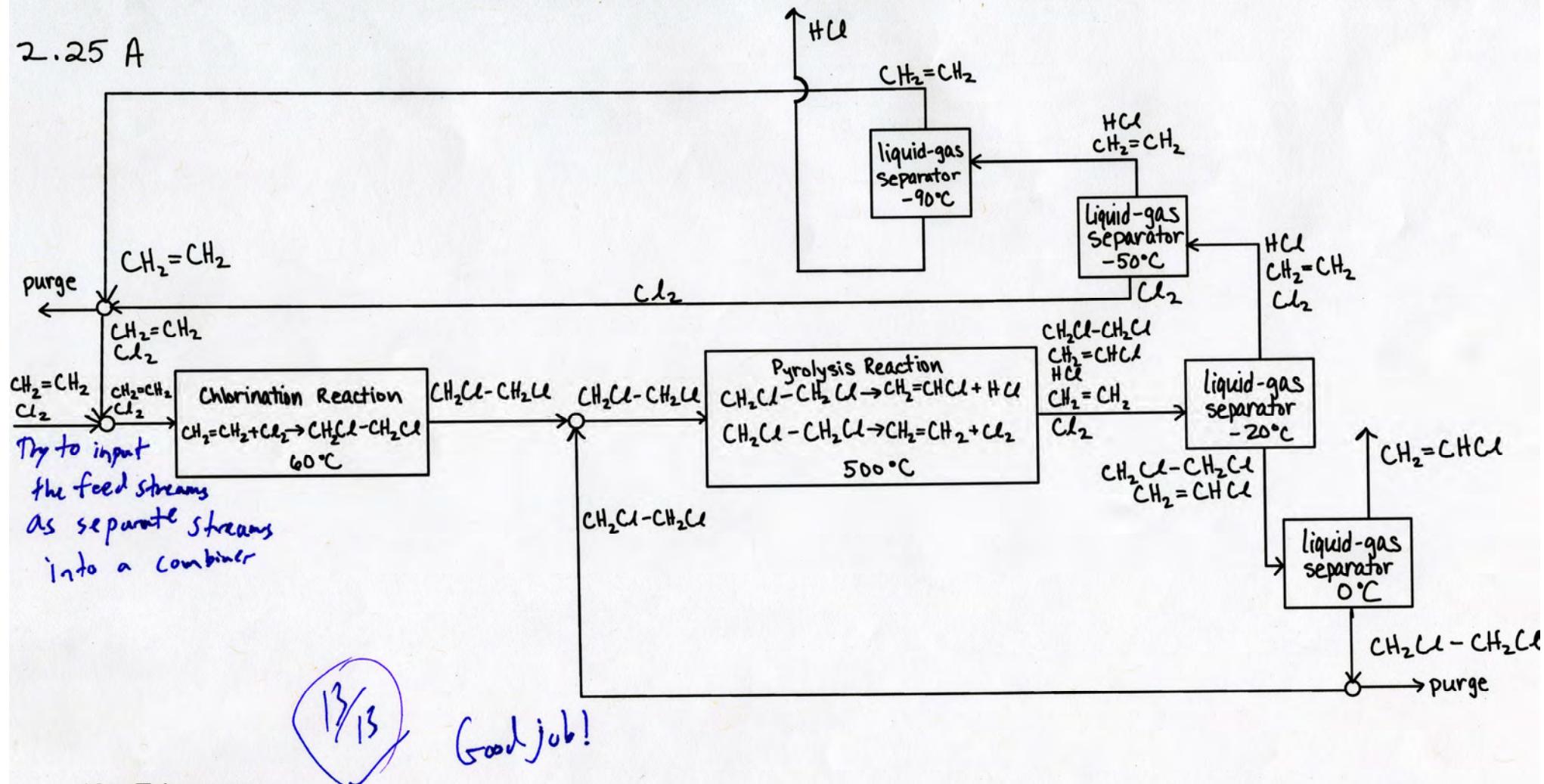


Homework 1 Excellence – exercise 2.25(A) – Team 18

Amber Belk (Coordinator), Dolly Hritz, Parth Vaidyanath

Team 18

2.25 A



Key Takeaways:

- You can have multiple reactions in a reactor.
- If there is another reaction that uses some of the product with a low conversion rate (i.e., 35%), it is not worth the extra process unit. *The extra reactions are cyclical so they are useless to use*
- When separating many compounds, it is better to separate the compounds approximately in half so that further separators are smaller.

EngrD 2190 – Lecture 8

- Homework 3 due Friday 9/19:

Formal mass balances:

exercises 3.12 and 3.28

Every equation must have an explicit source.

see posted solutions for exercises 3.4, 3.10, and 3.24 (calculation session 3) and exercise 3.44 (today's lecture).

Append a list of 'take-aways' to each exercise.

Process Design with qualitative, informal mass balances:

exercises 3.115 and 3.125

see posted solutions for exercises 2.36 and 3.126 (lecture 6), exercises 2.32 (calculation session 2), and 2.35 (calculation session 3).

Append a list of 'take-aways' to each exercise.

Start each solution on a separate page.

Requirements for Formal Mass Balances

- Define nomenclature.
- Show system borders and state assumptions.
- State source of equations. *Every equation must have an explicit source.*
examples: “apply conservation of mass” or “stream compositions”
or “process specification for washer”
- Describe derivation. “Substitute eqns (1) and (2) into eqn (3).”
- Box your answers. Numbers must have proper significant figures
and include units (e.g., kg/min).

Flow sheets for mass balance exercises are posted on-line.

Select the “Textbook” item at the EngrD 2190 homepage.

Exercise 2.35

2.35 Design a process to produce P from A . (Not the same A and P as in any other exercise.)

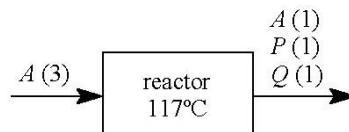


The reaction is reversible; P can be converted to A . A also reacts reversibly to form Q .

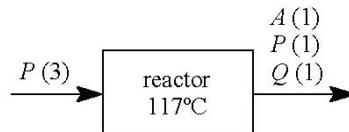


The reactions of A to form P and Q go to equilibrium, which is an equimolar mixture of A , P , and Q .

The example below shows the reactor effluent when pure A enters the reactor. The numbers in parentheses are flow rates, in mol/min.



Any composition of A , P , and Q entering the reactor will leave as an equimolar mixture of A , P , and Q . For example,



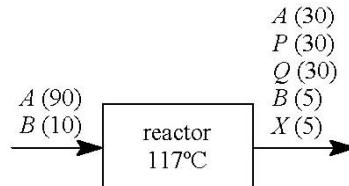
A is available only as a mixture of 90% A and 10% B . (All compositions in this exercise are in mol%). The reactor that converts A to P (and Q) also converts B to X .



Any composition of B and X entering the reactor will leave as an equimolar mixture of B and X .



In summary, 100 mol of feed entering the reactor will produce the following output.



Design Goals (in decreasing importance)

- Maximize the total value of the product(s).
- Minimize the *number* of units.
- Minimize the *size* of each unit.

Design Rules.

- Start with 100. mol/min of a 90:10 $A:B$ mixture.
- List the substances and *approximate* flow rates in every stream. One significant figure is sufficient.

Deductive

Inductive

Deductive

Inductive

Exercise 2.35 with deductive only

2.35 Design a process to produce P from A . (Not the same A and P as in any other exercise.)



The reaction is reversible; P can be converted to A . A also reacts reversibly to form Q .



The reactions of A to form P and Q go to equilibrium, which is an equimolar mixture of A , P , and Q .

A is available only as a mixture of 90% A and 10% B . (All compositions in this exercise are in mol%).) The reactor that converts A to P (and Q) also converts B to X .



Any composition of B and X entering the reactor will leave as an equimolar mixture of B and X .

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News Item

Walk this number of steps each day to cut your risk of dementia

By Sandee LaMotte, CNN, September 6, 2022

... People between the ages of 40 and 79 who took 9,826 steps per day were 50% less likely to develop dementia within seven years, the study found. Furthermore, people who walked with “purpose” – at a pace over 40 steps a minute – were able to cut their risk of dementia by 57% with just 6,336 steps a day.

The standard step length is 2.5 ft. The original study likely specified ‘walking with purpose’ a distance of 3 miles.

$$3 \text{ miles} \times (5280 \text{ ft/mile}) \div (2.5 \text{ ft/step}) = 6336 \text{ steps}$$

Try walking ‘without purpose’ – fewer than 40 steps per minute.

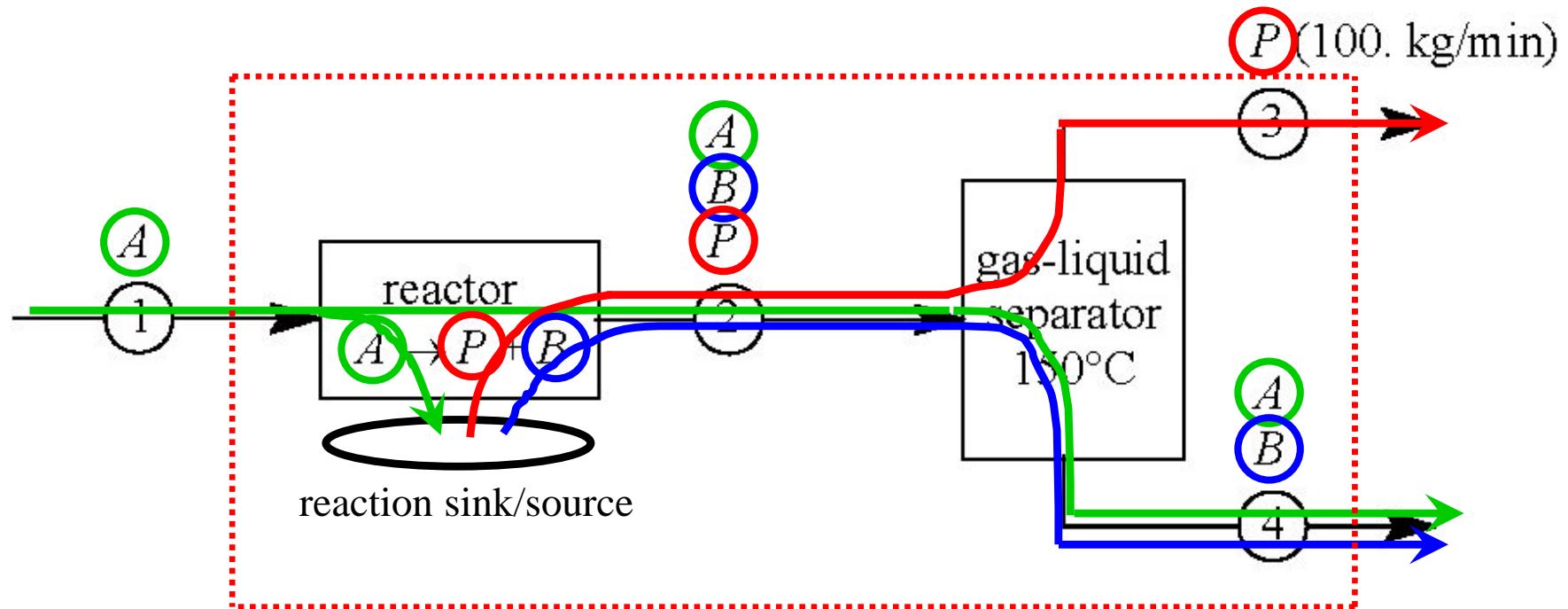
Options for Unreacted Reactants



	b.p.	
A	180°C	small ΔT ; difficult separation
B	181°C	large ΔT ; easy separation
P	120°C	

Scheme I. Avoid the expensive separator. Discard unreacted A with by-product B .

Model 1: one border should cross stream 3 - flow rate and composition given.



Model 1: $(3 \text{ streams}) \times (3 \text{ parameters/stream}) = 9 \text{ parameters}$

Calculate the flow rate and composition of stream 4. Calculate the flow rate of stream 1.

Scheme I is a simple process. It is tempting to calculate informally.

Instead, we will use this as an example of formal mathematically modeling.

A Formal Mathematical Model

Translate the process flowsheet to equations.

Identify a Physical Law or a Process Specification.

Translate to an equation.

Solve the equations.

Describe your method.

“Substitute equations (1) and (2) into equation (3).”

Show a logical mathematical progression.

$$2F_{T,1} + 32 = F_{T,2}$$

$$2F_{T,1} = F_{T,2} - 32$$

$$F_{T,1} = \frac{F_{T,2} - 32}{2}$$

Every equation must have an explicit source.

Model 1 of Scheme I – Mathematical Model

Choose a set of parameters. Choose 3 parameters from 4: total, A , B , and P .

1. Total and 2 components; probably total, A , and P .
2. 3 components; A , B , and P . ← arbitrarily choose this.

Translate the process flowsheet to equations.

Apply the Conservation of Mass to P . Write a mass balance on P .

rate of P in = rate of P out

$$F_{P,1} = F_{P,3} + F_{P,4}$$

$$0 \cancel{>} 100 + 0$$

Implies system with red borders and process at steady state.

If you choose to omit this equation, you must *explicitly* describe system borders and state assumptions.

What is wrong? Although mass is conserved, P is not.

Closed system:

A

initially

$A + B + P$

later

Model 1 of Scheme I – Mathematical Model, cont'd

Apply the Conservation of Mass to P . Write a mass balance on P .

rate of P in + rate P is created = rate of P out + rate P is consumed

Second option: explicitly list the source from which P is created and the sink to which P is consumed.

For $A \rightarrow P + B$,

rate of P in + rate of A in + rate of B in = rate of P out + rate of A out + rate of B out

Arbitrarily choose the second option.

$$F_{P,1} + F_{A,1} + F_{B,1} = F_{P,3} + F_{P,4} + F_{A,3} + F_{A,4} + F_{B,3} + F_{B,4} \quad (1)$$

Process Specifications: stream 1: $F_{P,1} = F_{B,1} = 0$ (2), (3)

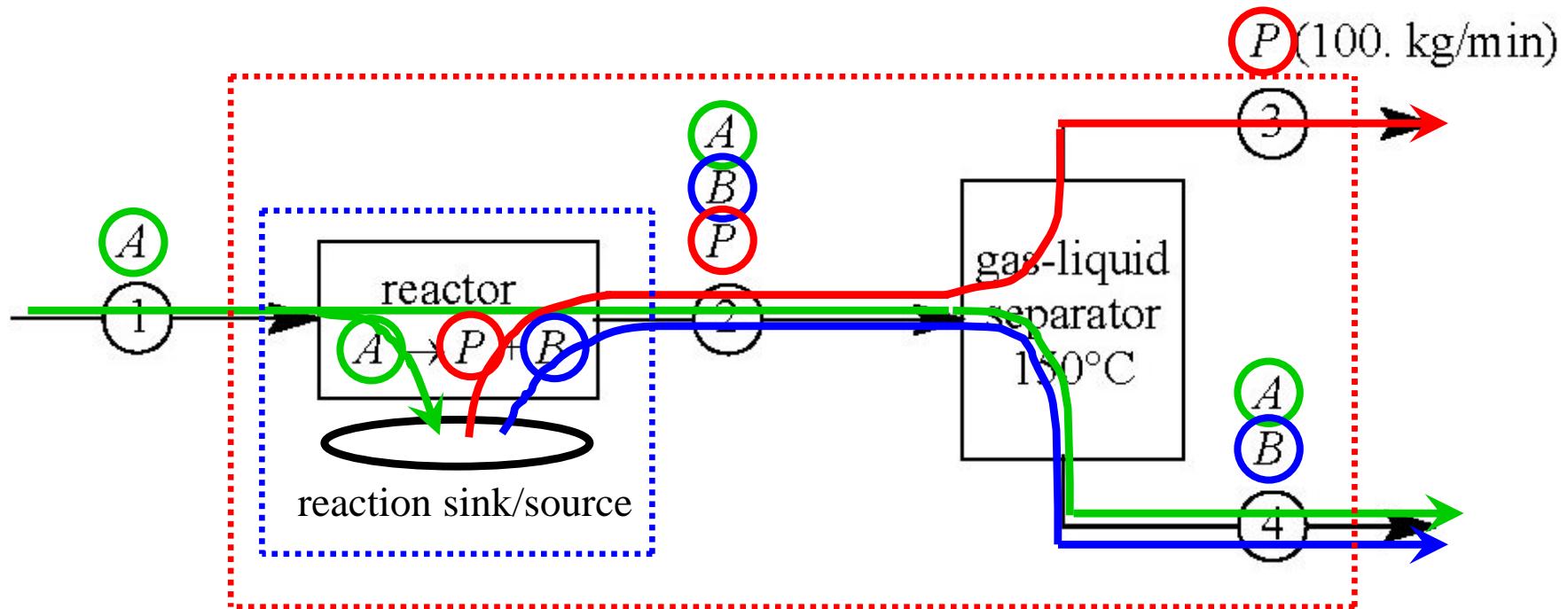
stream 3: $F_{A,3} = F_{B,3} = 0$, $F_{P,3} = 100$. (4), (5), (6)

stream 4: $F_{P,4} = 0$ (7)

9 parameters, 7 equations \Rightarrow need 2 more equations. *Consider the reactor.*

Scheme I. Avoid the expensive separator. Discard unreacted A with by-product B .

Model 1: one border should cross stream 3 - flow rate and composition given.



Model 1: $(3 \text{ streams}) \times (3 \text{ parameters/stream}) = 9 \text{ parameters}$

Calculate the flow rate and composition of stream 4. Calculate the flow rate of stream 1.

Model 2: $(2 \text{ streams}) \times (3 \text{ parameters/stream}) = 6 \text{ parameters}$

Model 2 of Scheme I – Mathematical Model

Reaction Specification: 60% of A reacts (40% does not) deductive

inductive: assume 100 kg of A enters reactor \Rightarrow 40 kg of A leaves the reactor.
 \Rightarrow 60 kg of $P + B$ leaves the reactor.

$$0.40F_{A,1} = F_{A,2} \quad (2.1)$$

$$0.60F_{A,1} = F_{P,2} + F_{B,2} \quad (2.2)$$

What are the relative masses of P and B created?

$$\text{mol wt } P = 2 \times (\text{mol wt } B) \quad \text{deductive}$$

If the mol wt of P is 100 amu, the mol wt of B is 50 amu inductive

If the mass of $P + B$ created is 150 kg, P is 100 kg and B is 50 kg.

If the mass of $P + B$ created is 60 kg, P is 40 kg and B is 20 kg.

$$F_{P,2} = 2F_{B,2} \quad (2.3)$$

Model 2 of Scheme I – Mathematical Model, cont'd

$$F_{P,2} = 2F_{B,2} \quad (2.3)$$

Equation (2.3) can also be obtained with a reactor mass balance.

rate of P in + rate P is created = rate of P out + rate P is consumed

$$\cancel{F_{P,1}}^0 + (2/3)(0.60F_{A,1}) = F_{P,2} + 0$$

$$0.40F_{A,1} = F_{P,2}$$

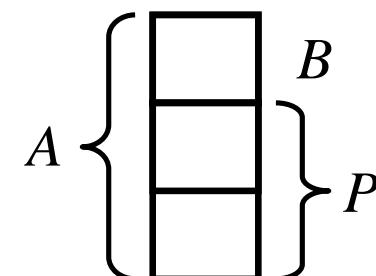
rate of B in + rate B is created = rate of B out + rate B is consumed

$$\cancel{F_{B,1}}^0 + (1/3)(0.60F_{A,1}) = F_{B,2} + 0$$

$$0.20F_{A,1} = F_{B,2}$$

$$F_{P,2} = 2F_{B,2} \quad (2.3) \quad \text{informal}$$

Equation (2.3) can also be obtained visually.



Model 3 of Scheme I

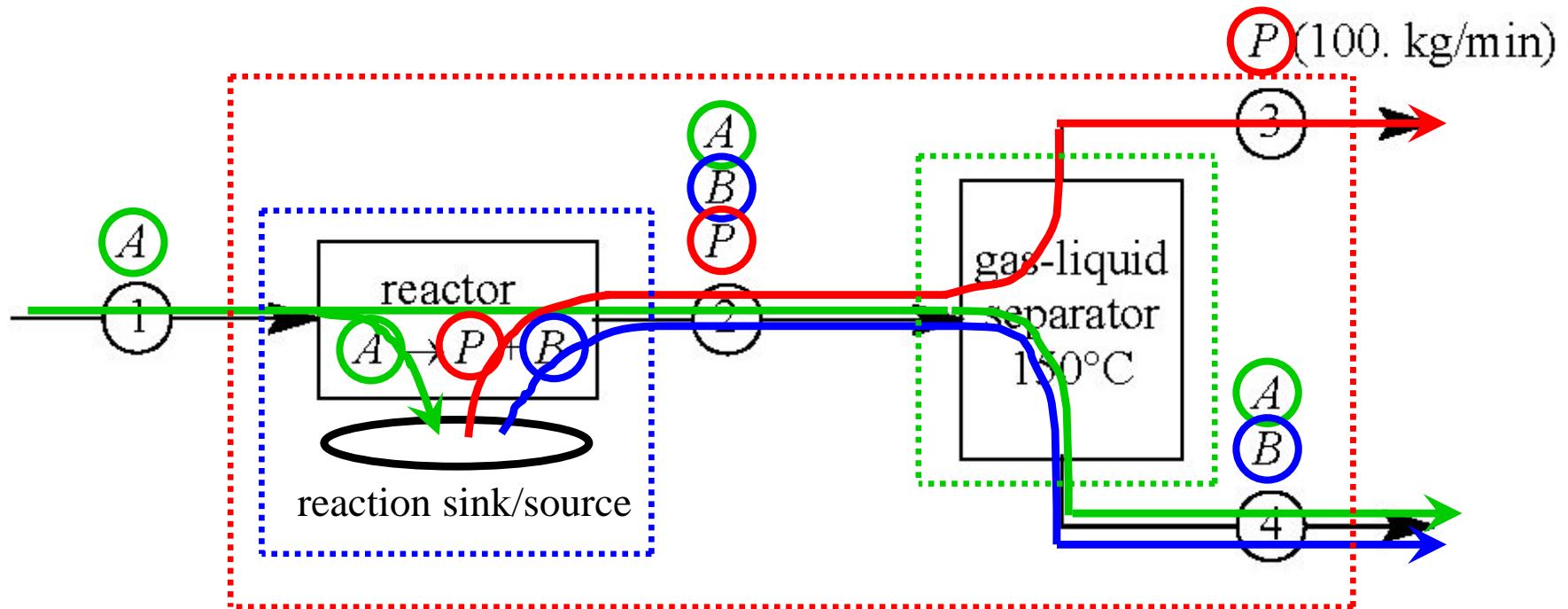
How to relate stream 2 (internal) to external streams?

We need a system with a border that crosses stream 2 and a border that crosses a known external stream.

Draw system borders around the separator.

Scheme I. Avoid the expensive separator. Discard unreacted A with by-product B .

Model 1: one border should cross stream 3 - flow rate and composition given.



Model 1: $(3 \text{ streams}) \times (3 \text{ parameters/stream}) = 9 \text{ parameters}$

Calculate the flow rate and composition of stream 4. Calculate the flow rate of stream 1.

Model 2: $(2 \text{ streams}) \times (3 \text{ parameters/stream}) = 6 \text{ parameters}$

Model 3: $(3 \text{ streams}) \times (3 \text{ parameters/stream}) = 9 \text{ parameters}$

Model 3 of Scheme I – Mathematical Model

Write a mass balance on the separator (note: no chemical reactions).

rate of A in = rate of A out

$$F_{A,2} = \cancel{F_{A,3}}^0 + F_{A,4} \quad (\text{informal})$$

$$F_{A,2} = F_{A,4} \quad (3.1)$$

Substitute equation (3.1) into equation (2.1).

$$0.4F_{A,1} = F_{A,2} \quad (2.1)$$

$$0.4F_{A,1} = F_{A,4} \quad (8)$$

Substitute equation (2.3) ($F_{P,2} = 2F_{B,2}$) into equation (2.2).

$$0.60F_{A,1} = F_{P,2} + F_{B,2} \quad (2.2)$$

$$0.60F_{A,1} = 2F_{B,2} + F_{B,2}$$

$$0.60F_{A,1} = 3F_{B,2} \quad (2.4)$$

Model 3 of Scheme I – Mathematical Model, cont'd

Write a mass balance on the separator (note: no chemical reactions).

rate of *B* in = rate of *B* out

$$F_{B,2} = \cancel{F_{B,3}}^0 + F_{B,4} \quad (\text{informal})$$

$$F_{B,2} = F_{B,4} \quad (3.2)$$

Substitute equation (3.2) into equation (2.4).

$$0.60F_{A,1} = 3F_{B,2} \quad (2.4)$$

$$0.60F_{A,1} = 3F_{B,4}$$

$$0.20F_{A,1} = F_{B,4} \quad (9)$$

We now have 9 equations for System 1 (borders around entire process).

Model 1 of Scheme I – Mathematical Model

$$F_{P,1} + F_{A,1} + F_{B,1} = F_{P,3} + F_{P,4} + F_{A,3} + F_{A,4} + F_{B,3} + F_{B,4} \quad (1)$$

$$\text{stream 1: } F_{P,1} = 0 \quad (2)$$

$$\text{stream 4: } F_{P,4} = 0 \quad (7)$$

$$F_{B,1} = 0 \quad (3)$$

$$0.4F_{A,1} = F_{A,4} \quad (8)$$

$$\text{stream 3: } F_{A,3} = 0 \quad (4)$$

$$0.2F_{A,1} = F_{B,4} \quad (9)$$

$$F_{B,3} = 0 \quad (5)$$

$$F_{P,3} = 100. \quad (6)$$

Substitute equations (2)-(7) into equation (1).

$$0 + F_{A,1} + 0 = 100 + 0 + 0 + F_{A,4} + 0 + F_{B,4}$$

$$F_{A,1} = 100 + F_{A,4} + F_{B,4} \quad (10)$$

Use equations (8) and (9) to substitute for $F_{A,4}$ and $F_{B,4}$ in equation (10).

$$F_{A,1} = 100 + 0.4F_{A,1} + 0.2F_{A,1}$$

$$(1 - 0.6)F_{A,1} = 100$$

$$F_{A,1} = 250 \text{ kg/min}$$

Model 1 of Scheme I – Mathematical Model, cont'd

From the previous slide, $F_{A,1} = 250 \text{ kg/min}$

Use equation (8) to calculate $F_{A,4}$.

$$F_{A,4} = 0.4F_{A,1} \quad (8)$$

$$F_{A,4} = 0.4(250) = 100 \text{ kg/min}$$

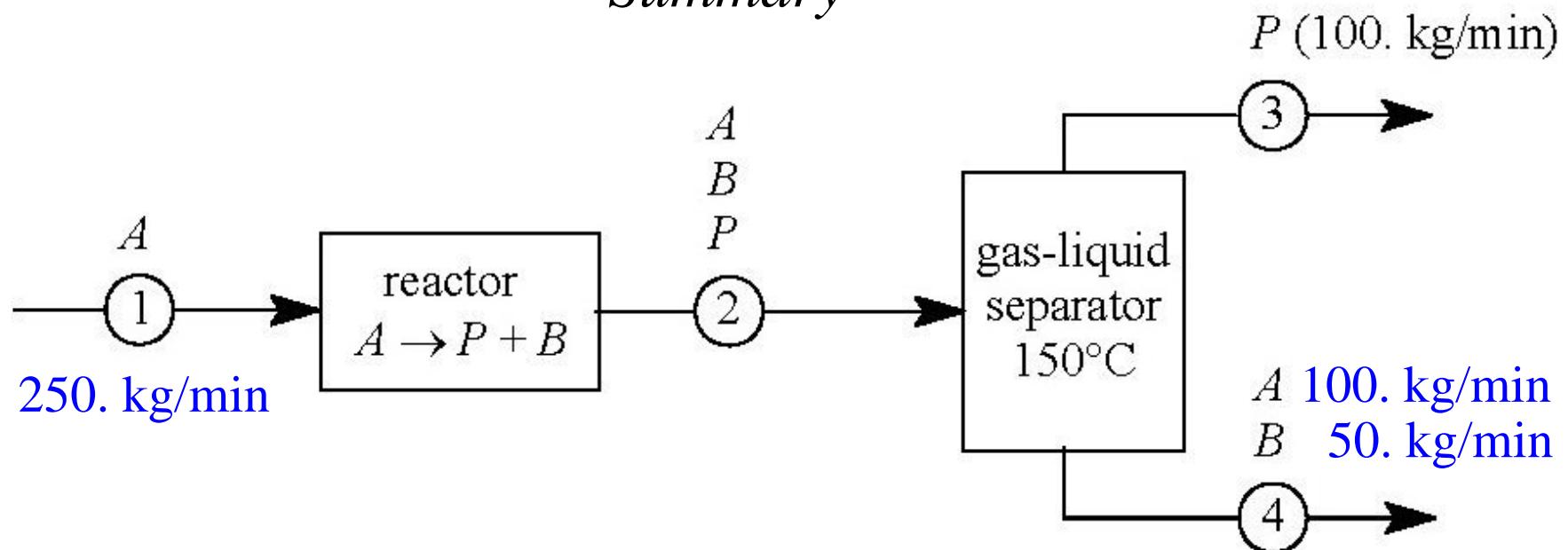
Use equation (9) to calculate $F_{B,4}$.

$$F_{B,4} = 0.20F_{A,1} \quad (9)$$

$$F_{B,4} = 0.20(250) = 50 \text{ kg/min}$$

Scheme I. Avoid the expensive separator. Discard unreacted A with by-product B.

Summary



Check Overall mass balance okay? In: 250 kg/min

Out: $100 + 100 + 50 = 250 \text{ kg/min}$ ✓

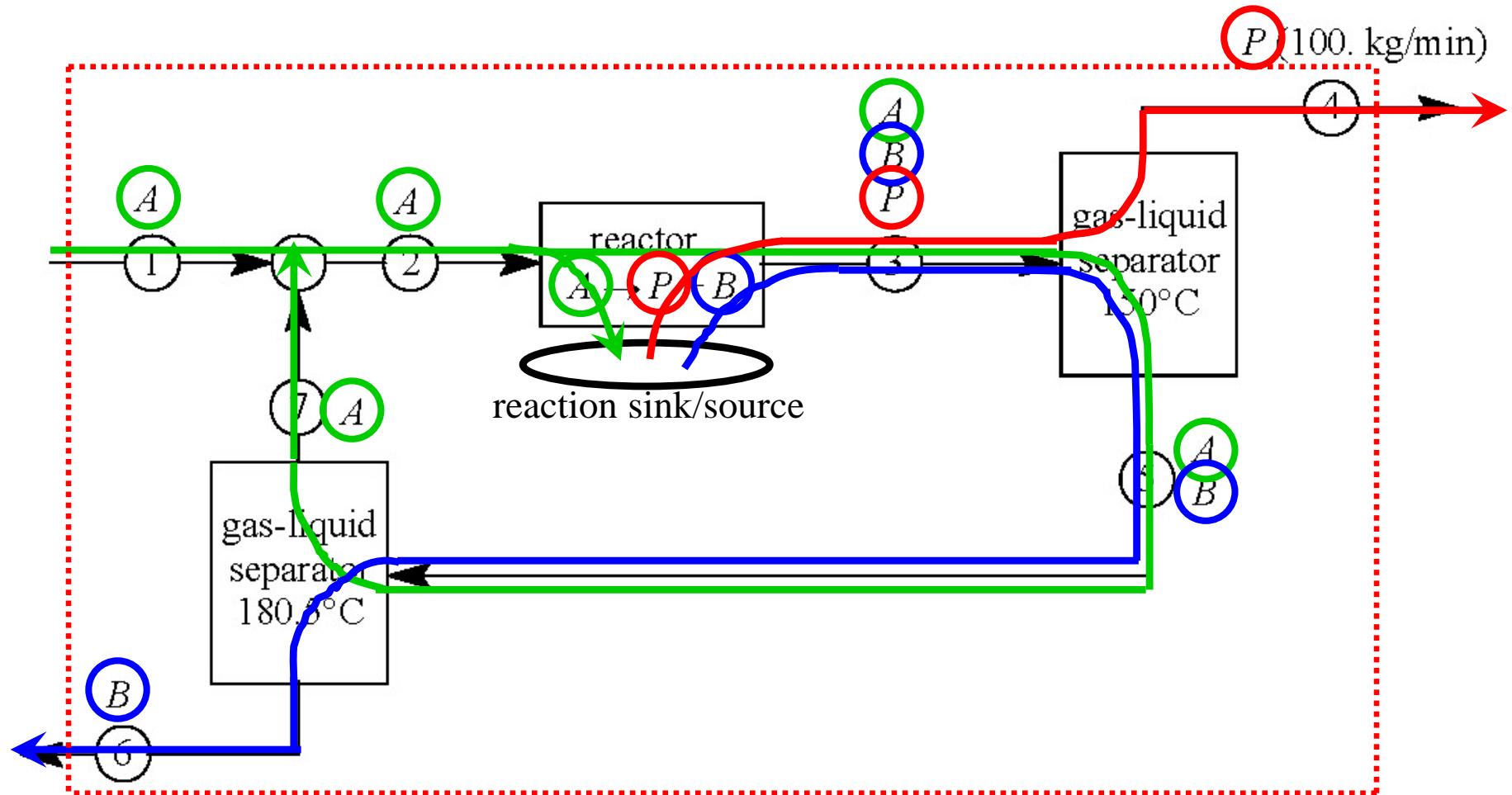
Mass ratio of P to B equals 2:1? P out = 100 kg/min

B out = 50 kg/min ✓

Scheme I is part (A) of exercise 3.44.

Solution is posted.

Scheme II. Separate unreacted *A* from by-product *B* and recycle *A*.



Model 1: (3 streams) \times (3 parameters/stream) = 9 parameters

Calculate the flow rates of streams 1 and 6, in kg/min. Calculate the flow rate and composition of stream 3.

Model 1 of Scheme II – Mathematical Model

Write a mass balance:

rate of *P* in + rate of *A* in + rate of *B* in = rate of *P* out + rate of *A* out + rate of *B* out

$$F_{P,1} + F_{A,1} + F_{B,1} = F_{P,4} + F_{P,6} + F_{A,4} + F_{A,6} + F_{B,4} + F_{B,6} \quad (1)$$

Process Specifications: stream 1: $F_{B,1} = F_{P,1} = 0$ (2), (3)

stream 4: $F_{A,4} = F_{B,4} = 0$, $F_{P,4} = 100$. (4), (5), (6)

stream 6: $F_{A,6} = F_{P,6} = 0$ (7), (8)

We need a 9th equation.

Because only *A* enters the reactor, a mass balance on the reactor yields the analogous result as Scheme I:

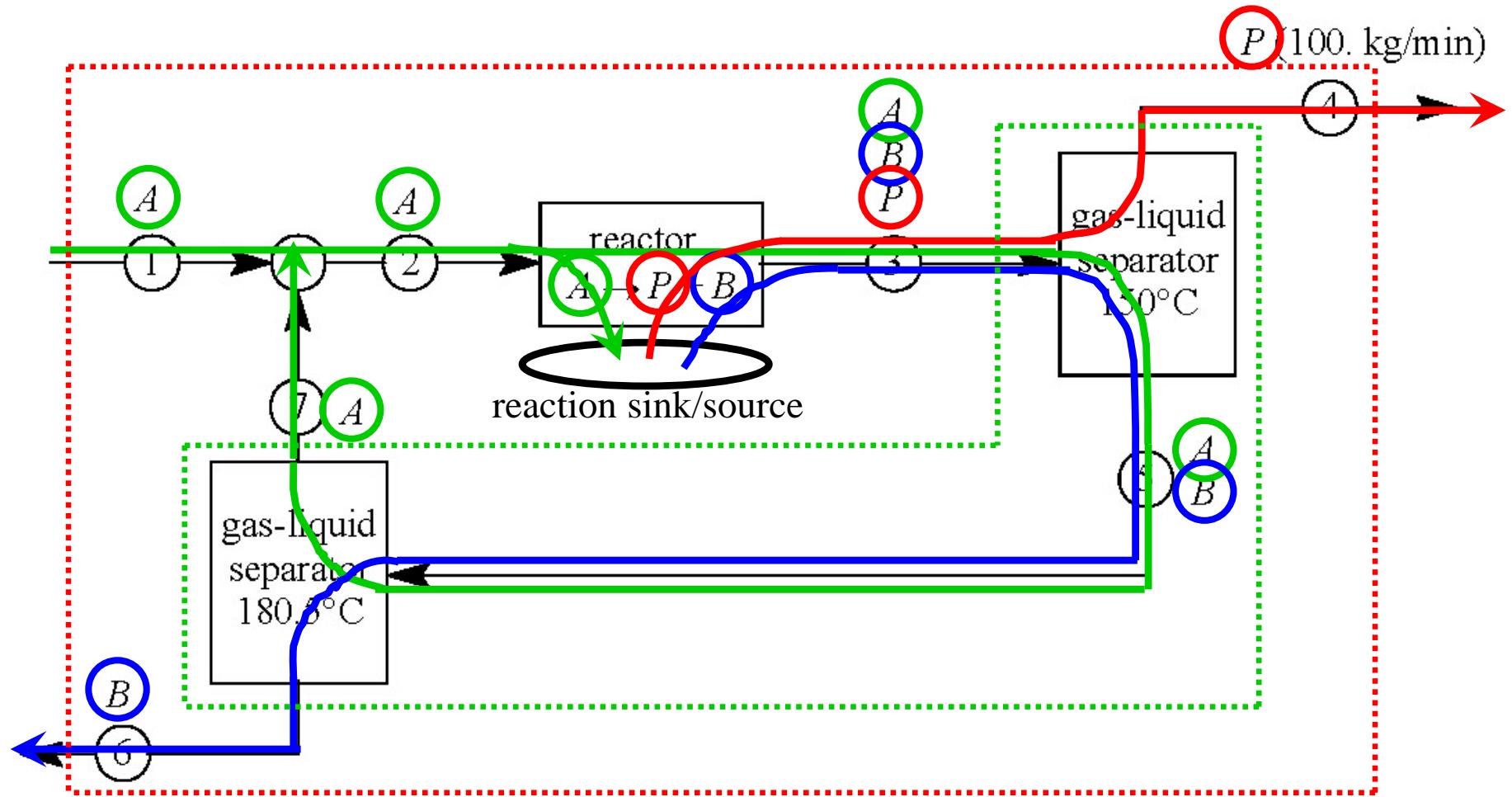
$$0.6F_{A,2} = F_{B,3} + F_{P,3} \quad (2.1)$$

$$F_{P,3} = 2F_{B,3} \quad (2.2)$$

Again we need a system with borders that cross internal streams.

Draw system borders that enclose both separators.

Scheme II. Separate unreacted *A* from by-product *B* and recycle *A*.



Model 1: (3 streams) \times (3 parameters/stream) = 9 parameters

Calculate the flow rates of streams 1 and 6, in kg/min. Calculate the flow rate and composition of stream 3.

Model 2: (4 streams) \times (3 parameters/stream) = 12 parameters

Model 2 of Scheme II – Mathematical Model

Write a mass balance on P (note: no chemical reactions).

rate of P in = rate of P out

$$F_{P,3} = F_{P,4} + \cancel{F_{P,6}^0} + \cancel{F_{P,7}^0} \quad (\text{informal})$$

$$F_{P,3} = F_{P,4} \quad (3.1)$$

Write a mass balance on B (note: no chemical reactions).

rate of B in = rate of B out

$$F_{B,3} = \cancel{F_{B,4}^0} + F_{B,6} + \cancel{F_{B,7}^0} \quad (\text{informal})$$

$$F_{B,3} = F_{B,6} \quad (3.2)$$

Substitute equations (3.1) and (3.2) into equation (2.2).

$$F_{P,3} = 2F_{B,3} \quad (2.2)$$

$$F_{P,4} = 2F_{B,6} \quad (3.3)$$

Model 2 of Scheme II – Mathematical Model, cont'd

Substitute equation (6) ($F_{P,4} = 100 \text{ kg/min}$) into equation (3.3).

$$F_{P,4} = 2F_{B,6} \quad (3.3)$$

$$100 = 2F_{B,6}$$

$$F_{B,6} = 50. \text{ kg/min} \quad (3.4)$$

Substitute equations (2)-(8) and (3.4) into the overall mass balance (equation 1).

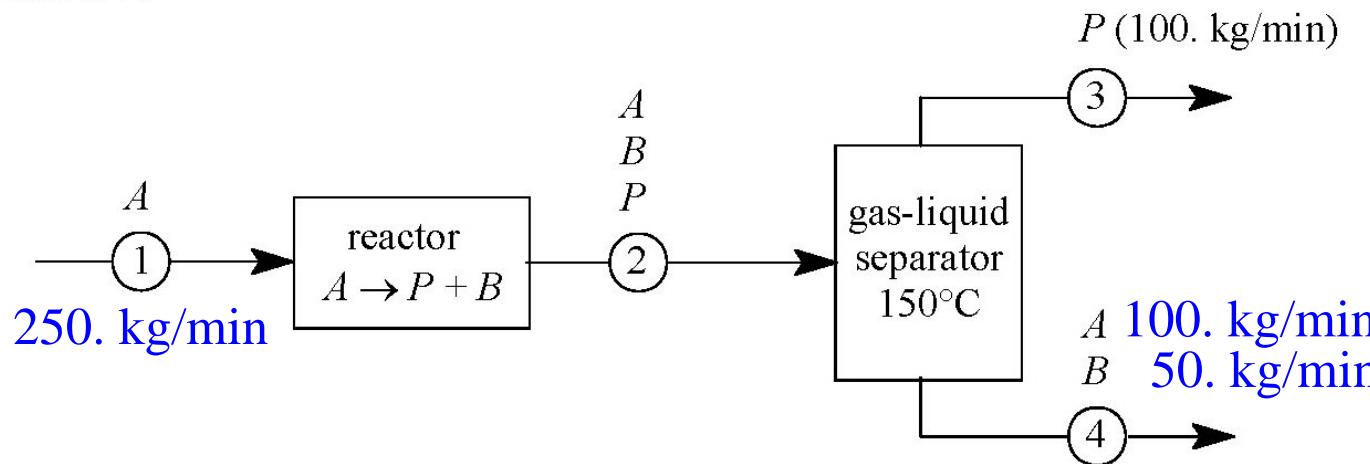
$$F_{P,1} + F_{A,1} + F_{B,1} = F_{P,4} + F_{P,6} + F_{A,4} + F_{A,6} + F_{B,4} + F_{B,6} \quad (1)$$

$$0 + F_{A,1} + 0 = 100 + 0 + 0 + 0 + 0 + 50$$

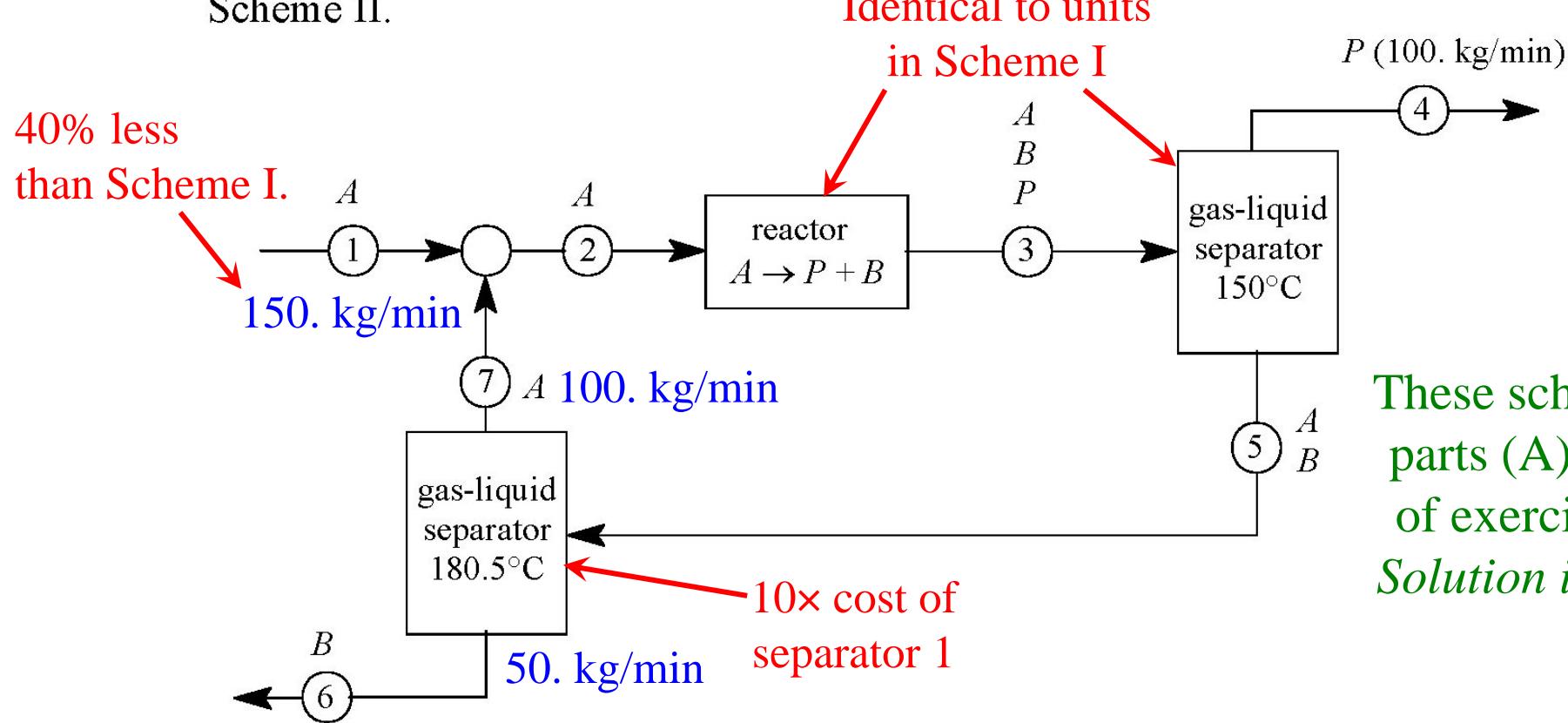
$$F_{A,1} = 150 \text{ kg/min}$$

Summary of Schemes I and II.

Scheme I.



Scheme II.



These schemes are parts (A) and (B) of exercise 3.44.
Solution is posted.